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# **Removal Of BTX From Aqueous Solutions by Adsorption Using PDMS Foar**



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# Abstract

Due to untreated wastewater disposal from a growing population and industry, biological and chemical pollutants have accumulated in the environment. Benzene, toluene, and xylene (BTX) are among the most frequently encountered contaminants in industrial wastewater. Due to their toxic and carcinogenic nature, BTX-containing industrial wastewater requires proper treatment prior to discharge to open water. This study examined the monocomponent adsorption of BTX from an aqueous solution using polydimethylsiloxane (PDMS) foam. Adsorption performance was optimised under various experimental conditions, including the effects of contact time, adsorption dosage, and initial concentration. The adsorption capacity of PDMS foam followed the order X > T > B, and the equilibrium of adsorption was reached in 6 h. The adsorption isotherms were analysed using the Langmuir, Freundlich, and Temkin models to evaluate their suitability for fitting the experimental data. The kinetics of the process were assessed employing both the pseudo-first-order and pseudo-second-order models. The adsorption data exhibited a good fit with Freundlich isotherms and a pseudo-second-order kinetic model. Based on experimental findings, PDMS foam shows great promise as an effective adsorbent for removing BTX from water.

Keywords: PDMS foam; gas foaming process; BTX removal; adsorption isotherm; adsorption kinetic.

## Introduction

Access to freshwater is essential for the sustenance of humans and wildlife. Despite the fact that approximately 97.5% of the Earth's total water resources are comprised of seawater, there remains a significant shortage of freshwater for human use. This shortage causes a significant challenge to communities worldwide. Access to safe drinking water is essential for promoting overall health and well-being. Individuals face heightened risks of waterborne diseases and other health complications without adequate access to clean water. As a result of the rapidly growing population and industrial activity, biological and chemical pollutants have accumulated in the environment due to the disposal of untreated wastewater [1,2]. The pharmaceutical industry, along with sectors including detergents, plastics, inks, paints, and adhesives, significantly contributes to the contaminant concentrations in wastewater. The disposable wastes of these industries contain petrochemical materials such as BTX, which refers to benzene, toluene, and xylene as they are used as starting materials. [3–5] Even at low concentrations, BTX is detrimental to human health on account of its exceptionally high toxicity and carcinogenic characteristics. Additionally, leukaemia, fatal deficiencies of the nervous system, and irritation of the skin, eyes, and mucous membranes may result from BTX exposure [3,6–9]. Thus, removing such harmful pollutants from wastewater is a critical global concern. The two main techniques applied to control BTX are destruction and recovery. Catalytic oxidation, thermal oxidation, and

biodegradation are examples of destruction techniques, while absorption, adsorption, and membrane separation are examples of recovery techniques [10–16]. The sorption process has been demonstrated to be both technically and economically effective for removing organic compounds from water.

\*Corresponding author e-mail: lialatawi@ut.edu.sa; (Lila Alatawi). Receive Date: 26 June 2024, Revise Date: 08 August 2024, Accept Date: 18 August 2024 DOI: 10.21608/ejchem.2024.299520.9906 ©2025 National Information and Documentation Center (NIDOC) Various sorbents, such as commercial organoclay [10], activated sludge [17], activated carbon [18], and periodic mesoporous organosilica [19], have been used in the removal of BTX from wastewater. However, there are some difficulties in using these sorbents, such as complex preparation, low working capacity, and low recyclability. Moreover, removing sorbents from the solution requires pre-treatment methods like centrifugation or filtration, which limit large-scale application. Thus, there is a strict necessity to develop cost-effective, non-toxic, and eco-friendly adsorbents.

Recently, there has been a lot of interest in porous polymeric materials like polydimethylsiloxane (PDMS) due to their excellent characteristics. PDMS foam has many applications in different fields because of its hydrophobicity, simple fabrication, low cost, remarkable reusability, large surface area, high flexibility, elasticity, and thermal stability. Some of its applications include sensors, microfluidics, adsorbents, absorbents, and oil/water separation [20–23]. PDMS foams have been manufactured using various methods, including porogen leaching [21,24–34], gaseous blowing agents [1,35,36], and emulsion techniques [37–43]. However, the porogen leaching approach requires toxic solvents and a long processing time. On the other hand, the surfactants used in the emulsion method must be eliminated because they affect the quality of the foam.

Additionally, studies that employed the gas blowing approach to generate PDMS foam either coupled it with other techniques or added more hazardous substances, making the process more complicated, time-consuming, and non-eco-friendly.

This work introduces a fast, easy, and effective method for preparing PDMS foam via gas foaming. There is minimal work available in the literature on the formation of PDMS foam using this method. Most reported works employed HCl and HNO<sub>3</sub> as catalysts. For the first time, this work explored using green materials, namely acetic acid as a catalyst and NaHCO3 as a blowing agent, to produce PDMS foam. This process has minimal environmental impact, as no waste materials result from the preparation process. It is hypothesised that the foam has excellent selectivity, ensuring it only adsorbs the desired contaminants, leaving the surrounding water or environment unaffected, making it suitable for large-scale applications.

# **Materials and Methods**

Materials

A Sylgard-184 kit from Dow Corning is provided in two components: Sylgard-184 A (base) and Sylgard-184 B (curing agent). Acetic acid and sodium bicarbonate were purchased from R&M Chemicals. Benzene with 99.5% purity, toluene with 99% purity, and mixtures of isomers of xylene with 98.5% purity were obtained from System Chemicals.

## **Preparation of PDMS foams**

The PDMS foam was prepared based on prior work [44]. First, the PDMS base and curing agent were combined in a 10:1 mass ratio, thoroughly mixing until a homogeneous prepolymer liquid formed. Then, sodium bicarbonate was added at 5% by weight and acetic acid at 10% by weight to the PDMS prepolymer. The mixture was stirred manually until it was uniform and the sodium bicarbonate was fully dispersed. The mixture was placed in a preheated oven at 100 °C, curing for one hour. After curing, the mould was removed from the oven, allowed to cool to room temperature, and then the formed PDMS foam was extracted. The foams were washed with water to remove any residual chemicals and allowed to air dry completely before further use.

#### Characterisation

The foam morphology was examined using a field emission scanning electron microscope (FE-SEM JEOL JSM-7600F, Tokyo, Japan). The obtained SEM images were analysed using Fiji/ImageJ software, V 1.8.0. The FTIR spectra were acquired on the Thermo Fisher Scientific Nicolet iS10 spectrometer, USA, in the region of 400–4000 cm<sup>-1</sup>.

## **Adsorption experiments**

B, T, and X adsorption from aqueous solutions onto PDMS foams in mono-component systems was carried out via batch adsorption in gas-tight glass vials. Each vial contained the adsorbent (0.2 g) and the adsorbate solution (40 mL) with different concentrations at room temperature. Each experiment was carried out in triplicate. A blank experiment was also performed in the absence of the adsorbent to evaluate and determine any potential loss of BTX due to volatilisation. The influence of key adsorption parameters (the amount of adsorbent used, the time of contact, and the initial concentration) on the uptake behaviour of BTX on PDMS foam was explored.

The impact of contact time was examined at varying intervals within the range of 15-360 minutes. To assess the influence of adsorbent dosage, the amount of PDMS foam was varied from 0.04 to 1.4 g/40 mL on 100 ppm of B, T, and X solutions at 25 °C for six hours. The impact of the initial BTX concentration on the uptake process was examined by altering the concentrations within the range of 50 to 500 mg/L for B and T and from 30 to 150 mg/L for X. The total time needed to reach equilibrium for adsorption was six hours.

A Lambda 35 UV-Vis spectrophotometer (PerkinElmer Life) was used to determine the adsorbate concentration at the respective maximum wavelengths ( $\lambda_{max}$ ) of 254 nm, 261 nm, and 264 nm for B, T, and X. The adsorption capacity of BTX by PDMS foam was obtained by Equations (1)

$$q_e(\text{mg/g}) = \frac{(c_0 - c_e)V}{m}$$
(1)

The removal efficiency of BTX by PDMS foam was obtained by Equations (2)

$$\% R = \frac{c_0 - c_e}{c_0} \times 100 \tag{2}$$

where  $q_e (mg/g)$  is the adsorption capacity at equilibrium,  $C_0 (mg/L)$  and  $C_e (mg/L)$  represent the initial and equilibrium concentrations of BTX, respectively, m (g) is the mass of PDMS foam, and V (L) represents the volume of the BTX solution.

#### Adsorption isotherm

The adsorption isotherm describes the equilibrium between the concentration of an adsorbate in a solution and the amount of that adsorbate adsorbed onto a solid surface. The adsorption isotherm shape reflects the solute's adsorption behaviour and the adsorbent's surface properties. The most commonly used adsorption isotherms are the Langmuir, Freundlich, and Temkin models, extensively studied and applied in various areas, such as environmental research, biotechnology, and materials science [45,46]. For the study of the adsorption isotherms, three different models were utilised in their linear form:

the Langmuir model (Equations 3)

the Freundlich model (Equations 4)

$$\ln(q_e) = \ln(K_F) + \frac{1}{n} \ln(\mathcal{C}_e) \qquad (4)$$

 $\frac{C_e}{q_e} = \frac{1}{q_{max}K_L} + \frac{C_e}{q_{max}}$ 

(3)

Temkin isotherm model (Equations 5)

$$q_e = B_1 \ln(K_T) + B_1 \ln(C_e) \qquad (5)$$

*Where:*  $q_{max}$  (mg/g): maximum adsorption capacity of BTX,  $K_L$ ,  $K_F$  and  $K_T$ : constants of Langmuir, Freundlich, and Temkin, respectively. Also, *n* and  $B_I$ : constants related to the intensity of the adsorption and adsorption heat, in that order [47–49].

## **Kinetic Studies**

Adsorption kinetics are mathematical expressions that explain the duration needed for the adsorption process to achieve equilibrium. Kinetic models can be used to make predictions about the behaviour of chemical reactions under different conditions. They are an essential tool for understanding the mechanisms of chemical reactions and also provide data for the design and modelling of this process [50–52]. Two distinct kinetic models were applied to analyse the kinetic batch experimental data:

The pseudo-first-order kinetic model (Equations 6)

$$\log(q_e - q_t) = \log(q_e) - K_1 \frac{t}{2.303}$$
(6)

The pseudo-second-order kinetic model (Equations 7)

$$\frac{\bar{t}}{q_t} = \frac{1}{K_2(q_e)^2} + \frac{t}{q_e}$$
(7)

*Where:*  $q_e$  (mg/g): adsorption quantity at equilibrium  $q_t$  (mg/g): adsorption amount at any time t (min),  $K_1$  (min<sup>-1</sup>) and  $K_2$  (g/mg.min): rate constants of the pseudo-first-order and pseudo-second-order, respectively [48,53].

# **Results and Discuss**

# **Preparation of PDMS foams**

The PDMS foam was produced through the gas-blowing process. Heating the mixture in the oven led to the crosslinking of the polymer (Figure 1). In addition, the decomposition of  $NaHCO_3$  and the reaction between acetic acid and  $NaHCO_3$  took place, releasing the  $CO_2$  gas responsible for the porous structures generated in the PDMS foam.

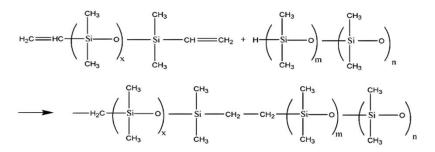


Fig. 1: Crosslinking reaction of PDMS foams [54]

# Characterisation

## Morphology

The morphology of the PDMS foam, synthesised using 2:1 NaHCO<sub>3</sub>:acetic acid ratios and cured at 100°C, exhibits homogeneous and uniform porosity (Figures 2A and B). The figures show connected micropores with diameters less than 100  $\mu$ m and spherical interconnected macropores with sizes between 100  $\mu$ m and 1000  $\mu$ m. The pore homogeneity may be

explained by the simultaneous emission of  $CO_2$  throughout the curing stage, resulting in the simultaneous generation of cells and making the pores in the foam uniform. Figure 2 (C) shows the foam pore-size distributions determined based on the FESEM image. Most of the pores are less than 600  $\mu$ m in diameter, with a peak between 100  $\mu$ m and 200  $\mu$ m.

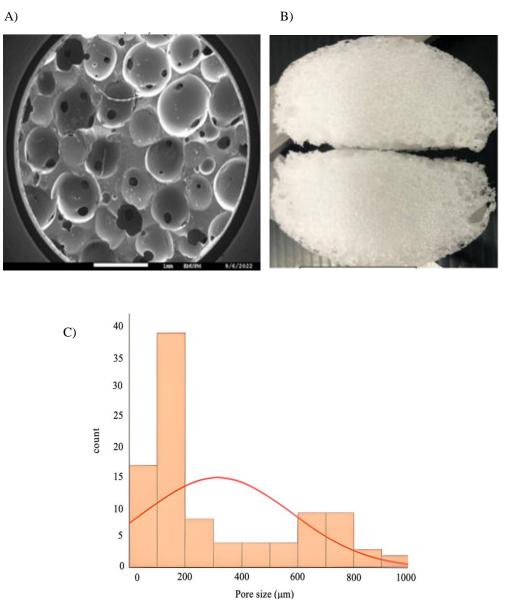


Fig. 2 A) FESEM photograph of PDMS foams. B) Photograph of of PDMS foam. C) pore size distribution of PDMS foam.

# Fourier transform infrared spectroscopy (FTIR)

The functional groups present in the foam were determined through analysis of the FTIR spectra of the PDMS foam, as depicted in Figure 3. The significant peak at  $1009 \text{ cm}^{-1}$ , which is the distinctive peak of the backbone of PDMS foam, is attributed to the stretching of Si-O-Si bonds. The main absorption bands in the FTIR spectra of PDMS foam are illustrated in Table 1 [27,54,58].

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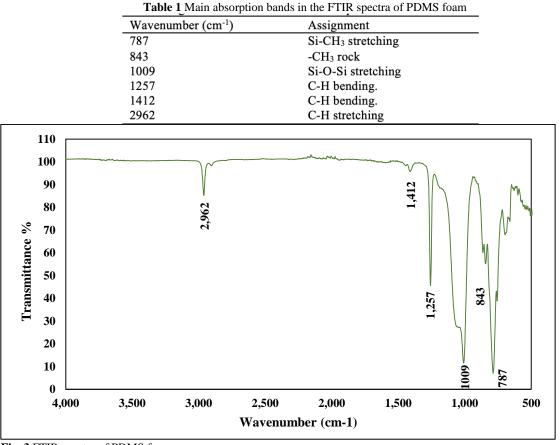


Fig. 3 FTIR spectra of PDMS foam

## Adsorption study

#### Effect of Contact Time

The influence of contact time on the adsorption of 100 mg/L of B, T, and X is illustrated in Figure 4. The adsorption capacities rapidly increased for the first 120 minutes due to the availability of vacant active sites, but increased slightly with increasing contact time as occupying the remaining adsorption sites became difficult due to repulsive forces between the adsorbate molecules adsorbed on the PDMS foam surface and those left in solution. After six hours, no significant changes in adsorption capacity indicated that the adsorption equilibrium was reached. The adsorption rate was in the order of X > T > B. This behaviour is attributed to several factors, namely solubility, the number of substituents, and the molecular size of BTX. The water solubility of BTX is in the order of X < T < B. As the least soluble compound, X is less surrounded by water molecules, making it easier to interact with the PDMS foam, leading to a higher adsorption capacity. The number of CH<sub>3</sub> substituents also increases from zero (B) to two (X), which in turn increases the molecular size of the compound (X > T > B). The larger the size of the molecules, the higher the interaction between the molecules and the PDMS foam, reflecting the adsorption rate order [59–63]. The increase of the methyl group (an electron-donating group) on the aromatic ring increases the electron density of the benzene ring, thus increasing the affinity of BTX to PDMS foam in the order X > T > B [59–63].

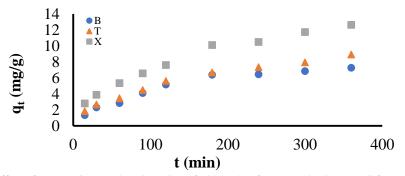


Fig. 4 The effect of contact time on the adsorption of 100 mg/L of B, T, and X by PDMS foam

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## **Effect of Adsorbent Dosage**

The dependence of B, T, and X adsorption capacity and adsorption efficiency on the PDMS foam dosage while maintaining other process variables constant is demonstrated in Figure 5, Figure 6, and Figure 7, respectively. The increase in the PDMS dosage led to a decrease in adsorption capacity, which was associated with the unsaturation of available active sites due to an increase in adsorbent dose at the same volume and concentration of BTX solution. However, the removal efficiency increases as the PDMS dosage increases. The increase in removal efficiency is associated with the increased availability of active sites. The intersection point in the graph is considered the optimum dose because it represents a balance between B removal efficiency and adsorption capacity. Hence, 0.2 g was selected as the optimum dose and was applied in further analyses.

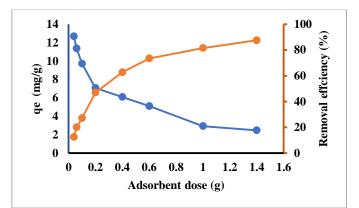


Fig. 5 Effect of adsorbent dose on the adsorption capacity of PDMS foam for the removal of B

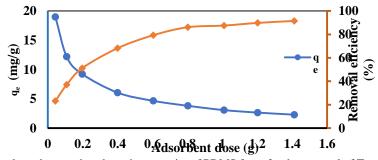


Fig. 6 Effect of adsorbent dose on the adsorption capacity of PDMS foam for the removal of T

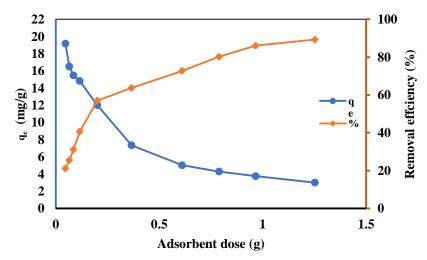


Fig. 7 Effect of adsorbent dose on the adsorption capacity of PDMS foam for the removal of X

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# **Effect of Initial BTX Concentration**

Figure 8 presents the impact of the initial BTX concentration on the adsorption capacity of PDMS foam. The  $q_e$  values increased with increasing adsorbate concentrations. Typically, this behaviour can be attributed to the increased driving force induced by the concentration gradient. As the BTX molecules in the solution increase, more BTX molecules surround the active sites of the PDMS foam, thus increasing the probability of BTX-PDMS interaction.

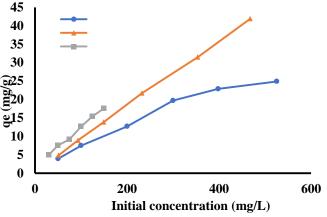


Fig. 8 Effect of initial BTX concentrate on the adsorption capacity of PDMS foam

## **Adsorption Isotherms Models**

Three isotherm models, namely, Langmuir, Freundlich, and Temkin isotherms, were examined to interpret an interaction of BTX with the PDMS foam. Figure 9 displays the adsorption isotherms, while Table 2 provides the related adsorption parameters. Based on the correlation coefficient R<sup>2</sup> values, the Freundlich model exhibited a better fit to the experimental data, meaning that the adsorption of BTX onto PDMS foam occurred at heterogeneous surfaces through a multilayer sorption system involving physical forces. The value of the parameter n in the Freundlich model indicates the favorability of the adsorption. Adsorption is favourable if the values of n are higher than unity. Therefore, BTX is favourably adsorbed by the PDMS foam, and their interaction is strong. The findings are compatible with other research studies [53,64]. The maximum adsorption capacity of several adsorbents for BTX is illustrated in Table 3.

	Table 2 Adsorption	parameters calculated from	Langmuir, Freundlich	. and Temkin isotherm models
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	Parameter	В	Т	Х
Langmuir	$q_{max}$ (mg/g)	46.948	243.902	23.529
	$\frac{K_L}{R^2} (L/mg) \ge 10^3$	3.02471	0.76756	35.76538
	$R^2$	0.9435	0.8839	0.8348
Freundlich	q <sub>max</sub> (mg/g)	37.682	75.102	26.688
	$q_{(exp)} (mg/g)$	25.605	45.460	17.593
	n	1.0972	1.0814	2.0032
	$\frac{\mathrm{K_F}\mathrm{mg/g(L/mg)}^{1/\mathrm{n}}}{\mathrm{R}^2}$	0.2603	0.2398	2.1878
	$R^2$	0.9939	0.9978	0.9967
Temkin	B <sub>1</sub> (J/mol)	8.665	13.279	4.762
	$K_T (L/g)$	0.043	16.576	2.282
	$\frac{K_{T}}{R^{2}} (L/g)$	0.9639	0.8677	0.8730

Table 3 The maximum adsorption capacity of various adsorbents for BTX

Adsorbent	Maximum adsorption capacity, q <sub>max (</sub> mg/g)			References
	В	Т	Х	
Thermally modified lignite	2.719	3.161	3.716	[53]
Zeolite Na-P1	0.032	0.0343	0.035	[65]
Smectite organoclay	0.52	0.69	0.75	[49]
Commercial Organoclay	0.938	2.765	14.865	[10]
Periodic mesoporous organosilica	0.6803	0.6207	0.6601	[19]
CNT sponge	0.13	2.45	14.31	[66]
PDMS foam	25.605	45.460	17.593	The present work

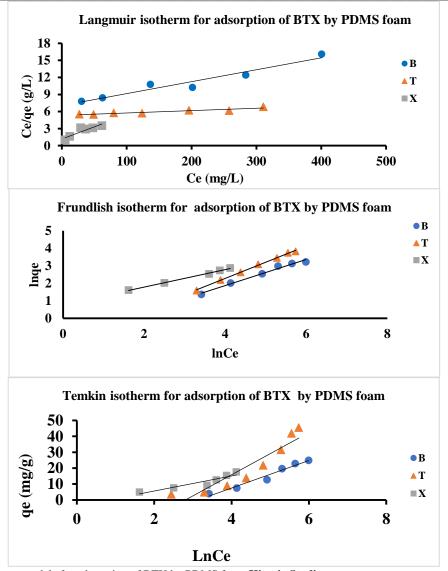


Fig. 9 Isotherm models for adsorption of BTX by PDMS foam Kinetic Studies

Figure 10 represents the linearised graph of a pseudo-second-order kinetic model for BTX. The parameters of the pseudosecond-order kinetic models for BTX are shown in Table 4. The correlation coefficient  $R^2$  values of pseudosecond-order are much closer to unity. Furthermore, the theoretical values  $q_{e(cal)}$  agree well with the corresponding experimental values  $q_{e(exp)}$ . Hence, the adsorption of BTX on PDMS foam is better described by the pseudo-second-order model. The findings are consistent with other research studies [64,65,67,68].

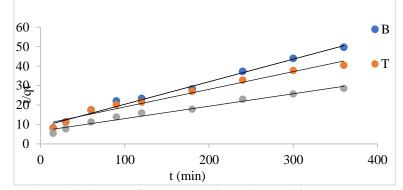


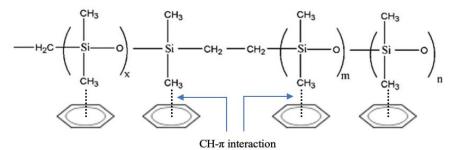
Fig. 10 Pseudo-second-order kinetic model for adsorption of BTX by PDMS foam

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Adsorbate Ini	Initial concentration	q <sub>e (exp)</sub>	q <sub>e (cal)</sub> (mg/g)	K <sub>2</sub> (g/mg.h)	Rate (mg/g.h)	R <sup>2</sup>
		al concentration C <sub>0</sub> (mg/L) (mg/g)				
	$C_0 (mg/L)$					
В	100	7.25	8.63	0.001521	0.1133	0.9874
Т	100	8.92	11.03	0.000827	0.1006	0.973
			15.63	0.000619		0.975

## Adsorption mechanism

The mechanism responsible for the adsorption of BTX on PDMS foam can be identified as the CH  $-\pi$  interaction, which arises mainly from charge transfer between the PDMS methyl groups and the  $\pi$ - electrons of BTX (Figure 11). Methyl groups are electron-donating, meaning they can increase the electron density of the aromatic ring. The increased electron density in the aromatic ring can enhance the CH- $\pi$  interaction. In this interaction, the hydrogen atoms from CH groups on the PDMS foam can be attracted to the  $\pi$  electron cloud of the aromatic ring. The higher electron density in the aromatic ring makes it more attractive to the hydrogen atoms, strengthening the CH- $\pi$  interaction. In BTX compounds, X has two methyl groups, T has one, and B has none, resulting in X having the strongest CH- $\pi$  interaction with PDMS foam, followed by T and then B. Another potential interaction can be related to the hydrophobic nature of the PDMS foam, composed mainly of repeating dimethylsiloxane units, is hydrophobic due to its surface's abundance of methyl groups. Being of similar properties, the affinity of BTX towards the hydrophobic surface of PDMS foam resulted in a higher BTX-PDMS interaction and, thus, a higher adsorption capacity.



**Fig 11**: CH- $\pi$  interaction between a benzene molecule and PDMS foam

#### Conclusions

This paper investigated the adsorption of BTX onto PDMS foam from aqueous solutions. After six hours, adsorption equilibrium was achieved. The adsorption capacity increases in the order X > T > B. Due to the increase of the methyl group on the aromatic ring, the electron density increased, reinforcing the CH  $-\pi$  interaction between BTX and PDMS foam. The Freundlich model was found to exhibit a better fit to the experimental data, meaning that the adsorption of BTX onto PDMS foam occurred at heterogeneous surfaces through a multilayer sorption system involving physical forces. The kinetics results revealed that the adsorption of BTX onto PDMS foam was best represented by the pseudo-second-order model. PDMS foam may constitute an efficient and environmentally friendly adsorbent for BTX removal.

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