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**INVESTIGATING MEASURES TO INCREASE THE LIFESPAN OF  
CONCRETE COASTAL STRUCTURES IN THE NILE DELTA**

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**ABSTRACT**

In terms of the importance of enhancing concrete coastal structures exposed to chlorides, this study was initiated with the objective of increasing their lifespan. Two measures were proposed (i.e. to increase the thickness of the concrete cover or add Carbon Fiber Reinforced Polymer (CFRP) sheets). 27 R.C. specimens were investigated experimentally. The specimens were exposed to variable sodium chloride ratios by weight "salt cement ratio" (s/c) (i.e. 3:100 "3%", 3:50 "6%" and 1:10 "10%"). The specimens were prepared, cured, dried and tested. The Zagazig Structural Laboratory was set. Measuring devices were fixed and measurements were undertaken. Also, photos were captured and observations were documented. The strains, cracking load and cracking pattern were determined. The undertaken measurements, the shot photos and documented observations were analyzed; graphs relating the different parameters were plotted and were presented. It was found that these enhancement measures improved the behavior of the concrete specimens subjected to Chlorides which would most probably extend the lifespan of concrete coastal structures.

**الملخص العربي:**

فيما يتعلق بأهمية المنشآت الساحلية الخرسانية التي اغلب مشاكل تدهورها ينتج عن صداد صلب التسليح تم البدء في هذا البحث الذي يهدف الى اجراء دراسة معملية عن صداد صلب التسليح الناتج عن تواجد نسب عالية من املاح

الكلوريدات في الخلطة الخرسانية المستخدمة مع اقتراح أساليب في علاج وتقوية العينات المختبرة . تشمل الدراسة المعملية اختبار عدد 27 من الأعمدة الخرسانية المسلحة ذو نسبة مئوية من كلوريد الصوديوم . تم اختبار جميع الأعمدة حتى الانهيار . كما تم عرض و مناقشة النتائج التي تم الحصول عليها مع عمل دراسة لمعرفة مدى تأثير العوامل المتغيرة التي تم دراستها على تصرف الأعمدة المختبرة من حيث الاحمال و الانبعاج و شكل الشروخ والكسر و الاجهادات للخرسانة المسلحة و حديد التسليح . و اخيرا تم اقتراح و عمل توصيات عن كيفية تفاعل و حماية المنشآت الخرسانية المسلحة المتواجدة في المناطق الساحلية من تأثير وجود أملاح الكلوريدات في الاجواء المحيطة.

## 1. INTRODUCTION

Up-and-coming problems, facing the low-lying lands, necessitate the implementation of extra concrete coastal protection measures. Due to their high construction cost, durable structures with longer lifespan are required. This is attributed to the fact that concrete is mainly damaged by sea water effects and chemical damage (i.e. from chlorides). This process adversely affects concrete exposed to these damaging stimuli. The expansion of the corrosion products (iron oxides) of carbon steel reinforcement induces mechanical stress that can cause the formation of cracks and disrupt the concrete coastal structures. Flat fragments of concrete are detached from the concrete mass and may fall down.

In terms of the importance of constructing longer lifespan concrete coastal structures, this research was initiated. The *main objectives* were to propose and examine the efficiency of the measures to enhance the structural behavior of coastal concrete structures (i.e. columns) when exposed to high percentages of sodium chloride. Additionally, the research aimed to determine the strain in steel so as strain of concrete, the buckling and the cracking so as ultimate loads of the enhanced specimens.

In order to achieve the above objectives, *a methodology was planned*. The methodology phases were to assemble available literature in the field of concrete degradation and enhancement methods; propose enhancement measures; design an experimental program; prepare specimens; adjust measuring devices; execute tests varying the s/c ratio; undertake measurements; analyze the measurements, plot the results; interpret them and provide conclusions so as recommendations for further research.

## 2. PROBLEM DEFINITION

In the *Nile Delta* in Egypt, likewise in all low-lying lands all over the world, there is an emergent need to construct extra coastal structures to face the up-and coming problems. Additionally, there is an urgent need to enhance the coastal structures endurance to withstand the great challenges of the near future and to possess a longer lifespan. This is attributed to the fact that the low-lying lands in coastal zones are confronted by many challenges that would need plenty of extra coastal protection measures. Among these challenges are:

- **Global warming and sea level rise:** Effects of global warming are long-term significant changes in the expected patterns of average weather of any coastal region. The world average temperature would rise due to the greenhouse effect caused by increasing levels of carbon dioxide. This would cause melting of ice, changing the hydrological cycle (of evaporation and precipitation) and changing currents in the seas and air flows in the atmosphere. Consequently, the coast together with the coastal structures would suffer from the severe impacts of sea level rise. Global sea level is currently rising due to the thermal expansion of water in the oceans and the addition of water from ice sheets. Consequently, the low-lying coastal areas (i.e. *Nile Delta*), many of which are heavily populated, are at risk of flooding. The IPCC (2007) projected that by the 2080s, millions of people would experience floods every year due to sea level rise. This would necessitate the importance of constructing more coastal durable protection structures.

- **Wave action:** The wave action induces coastal sediment movements that cause shoreline changes. This might also acquire more protection works.
- **Land subsidence:** Subsidence is the motion of a surface as it shifts downward relative to a datum such as sea-level. Ground subsidence is of concern to coastal engineers, geologists, geotechnical engineers and surveyors. The subsidence of land typically occurs to low-lying lands such as the *Nile Delta*. This might also acquire extra protection works.
- **Exposure to Chlorides:** Concrete is mainly damaged by sea water effects and chemical damage (i.e. from chlorides). This process adversely affects concrete exposed to these damaging stimuli. The expansion of the corrosion products (iron oxides) of carbon steel reinforcement induces mechanical stress that can cause the formation of cracks and disrupt the concrete coastal structures. Flat fragments of concrete are detached from the concrete mass and may fall down. This might also acquire additional protection works.

Many other factors contribute in coastal zone changes which necessitates the establishment of extra coastal structures which by their turn need to be enhanced to face the oncoming conditions. Consequently, measures should be proposed to enhance the behavior of the coastal structures which usually deteriorates thus causing their failure.

### 3. REVIEWING THE LITERATURE

Published reports, periodicals and articles in scientific journals were assembled, reviewed, analyzed and comprehended. Based on the revised literature, it was found that many researchers are involved in investigating long-term durable concrete that could be safely implemented in marine structures, IPCC (2001) and (2007).

Based on this revision, the different investigated aspects were analyzed and categorized into groups. These groups covered coastal structures attacked by chlorides, corrosion effects on concrete, chloride-induced corrosion, factors affecting chloride resistance, chloride resistance tests, indirect measures, theoretical studies, experimental studies, extraction of chlorides, numerical modeling, thermal cracking, finite element numerical models, corrosion staining in concrete and minimizing corrosion of steel, Koch et al (2002), Zhang et al. (2002) and Tang et al. (2012).

The assembled literature indicated that corrosion and its effect on concrete, chloride-induced corrosion, factors affecting chloride resistance, chloride resistance tests, indirect measures, theoretical studies, extraction of chlorides, numerical modeling, thermal cracking, finite element numerical models, corrosion staining in concrete and minimizing corrosion of steel are methodically and logically mentioned in the assembled literature. It also indicated that the experimental investigations are not meticulously enclosed in the available literature and are bounded by some discrepancies which mean that more investigations are required. Therefore; it was decided to go further and execute experimental work.

### 4. PROPOSING ENHANCEMENT METHODS

It was thought that if the bars are properly installed and are located away from the concrete surface in contact with the air, damage could not occur easily. Additionally, it was further perceived that if the steel bars are protected by Carbon Fiber Reinforced Polymer (CFRP) sheets. CFRP is a Polymer Matrix Composite material reinforced by

carbon. It has low density of 114 lb/ft<sup>3</sup> (i.e. 1800 kg/m<sup>3</sup>). Consequently, steel damage could not occur easily.

Accordingly, two measures were proposed:

- The first measure was to increase the thickness of the concrete cover.
- The second measure was to introduce CFRP sheets to the specimens.

## 5. DESIGNING AN EXPERIMENTAL PROGRAM

An experimental program was designed. It encompassed 27 specimens (i.e. S1 to S27) that were divided into 3 groups (i.e. Group I, II and III), each encompasses 9 specimens (i.e. columns). The second and third groups were enhanced either by increasing the thickness of the concrete cover or introducing CFRP sheets to the specimens.

It is to be noted that the tested cross section was 200x 200 mm. The steel reinforcement was 4Ø12. The concrete cover was taken as 25 mm except for the enhanced groups; it was taken as 40 mm. The salt cement ratio, by weight was 3%, 6% and 10%, Table (1).

## 6. INSPECTING THE MATERIALS

The specimens were prepared from cement, salt (i.e. Sodium Chloride), water, reinforcement bars and water. The **cement** used in this study was locally manufactured Ordinary Portland Cement, photo (1). Upon delivery, the cement was emptied into plastic sacks and then stored in dry air in the laboratory. This was achieved in order to minimize the deterioration of cement during the investigations. The **fine aggregate**, photo (2), was dry natural sand and the coarse aggregate consisted of a mixture of rounded and crushed gravel with 20 mm maximum nominal size. Coarse aggregate was washed by water to dissolve any salts in the aggregate. **Sodium Chloride salt** was implemented as a source of chloride ions, photo (3). In order to avoid the effects of different chloride ions diffusion rates due to different cation, the salts were added to concrete by dissolving the different quantities as ratios (3:100, 3:50 and 1:10) (i.e. 3%, 6% and 10%) by weight of cement in mixing water before casting. The salt was stored in plastic sacks at dry air in the laboratory before using. The used **steel** was 12 mm diameter deformed high tensile and 8 mm normal mild steel as main longitudinal reinforcement and shear stirrups, respectively. Tension tests were carried out on three specimens of each type.

The mechanical properties of the implemented materials were tested and were determined. They all fell within the allowable values prescribed in the *Egyptian Code of Practice*.

## 7. PREPARING THE SPECIMENS

The mixing procedures of the unenhanced and enhanced specimens were carried out in the laboratory mixer, photo (4). The mixing process proceeded as follows:

1. The materials were mixed dry for two "2" minutes.
2. Water was added gradually to the dry mix and was moved persistently until a uniform color and shape were obtained to the control specimens. The salty mixing water with different percentage s/c=3, 6, 10% was added gradually to the unenhanced and enhanced specimens and mixing was continued until a uniform color so as shape were obtained.
3. In the prepared wooden formworks, photo (5), the concrete was cast over the steel reinforcement, photo (6).

4. Concrete columns were mechanically vibrated for one minute.
5. Formworks were removed after 24 hours and were subjected to natural air and wet spray to cure it, photo (7), on daily basis for 28 days after casting.

## 8. SETTING THE LABORATORY AND FIXING THE MEASURING DEVICES

After investigating the materials and preparing the specimens, the Structural Laboratory in ZagazigUniveristy, Faculty of Engineering, was set in order to inspect the prepared specimens.

The laboratory is equipped with a loading machine (i.e. loading frame, hydraulic universal machine), photo (8). The specimens were prepared in the laboratory and placed on the loading frame to be inspected and the designed test program was achieved.

Columns were loaded by load cell symmetrically at two “2” points over an effective span of 50 cm. Two Linear Variable Differential Transducer (LVDT) gauges were used to measure the deflection, one of them under the load and the second at the mid span of the column. Concrete strain gauges were used to measure strain of concrete, and steel strain gauges were used to measure strain of steel. All gauges were connected to the data logger to read measurements. The measuring devices (i.e. strain gauges) were fixed on the prepared specimens after being cured and dried. The strain gauges were arranged as shown in photo (9).

## 9. UNDERTAKING MEASUREMENTS

After fixing the measuring devices, measurements were undertaken. These measurements were strain in steel so as concrete together with loads corresponding to crack, yield and ultimate loads. Deflection measurements were undertaken, as well. Also, crack patterns were photographed.

The strain of steel was measured at the middle of the main steel bar (within the tension zone). The gauges (10 mm) were connected to a data logger.

The strain of concrete was measured at the middle of the upper face of columns (at the compression zone) by fixing the strain gauge (20 mm) to the concrete. The gauges were connected to the data logger.

Loads were recorded by the data logger with an increasing increment of 2 KN until the first crack appears (i.e. first crack load), yield occurred (i.e. yield load) and crushing occurred (i.e. ultimate load). Photo (10) is provided to indicate the specimens during testing.

The deflection was measured at three points, the first at mid span of columns, the second and third points were measured under the acting loads.

Cracks were tracked, traced and sketched on the column during loading to reach failure. Photos were shot to capture the shapes of cracks. Notes were recorded to identify kind of failure.

## 10. ANALYZING THE RESULTS AND PRESENTING THEM

The undertaken measurements, the shot photos and documented observations were analyzed. Graphs relating the different parameters were plotted. Only a sample is presented here, figures (1) to (9). This sample was tested with 10% s/c ratio. It was chosen as it has the highest tested salt cement ratio in order to indicate the results clearly.

Figures (1) to (3) represent the relation between the loads and buckling for the unenhanced specimens and enhanced specimens with 40 mm cover or with CFRP sheets, respectively. Figures (4) to (6) represent the relation between the loads and strain of steel for the unenhanced and enhanced specimens with 40 mm cover or with CFRP sheets, respectively. Figures (7) to (9) represent the relation between the loads and strain of concrete for the unenhanced and enhanced specimens with 40 mm cover or with CFRP sheets, respectively.

Although the curves are self-explanatory curves, a comparison to the values of buckling, strain of steel and strain of concrete of the unenhanced specimens, enhanced specimens with 40 mm cover and enhanced specimens with CFRP sheets is given in table (2). It is to be noted that these values are a load of 400 KN (i.e. average load). The table also provides the enhancement percentage due to the provided extra concrete cover or the addition of CFRP.

Where:

$$\text{Enhancement percentage} = \frac{[\text{Value of unenhanced specimen} - \text{Value of the enhanced specimen}] \times 100}{\text{Value of unenhanced specimen}}$$

Also, photos (11) and (12) are given to illustrate the failure modes of unenhanced and enhanced specimens, respectively.

## 11. CONCLUSIONS AND RECOMMENDATIONS

Based on the executed experiments, conclusions were reached. The deduced conclusions are presented here, as follows:

- The unenhanced concrete specimens behaved differently from the enhanced specimens when they were exposed to chlorides.
- The unenhanced concrete specimens were easier to crush and crack at higher s/c ratio.
- The enhanced specimen experienced relatively lower buckling than the unenhanced specimens (i.e. enhancement percentage at 400 KN = 6 to 28%).
- The enhanced specimen experienced relatively less strain of steel than the unenhanced specimens (i.e. enhancement percentage at 400 KN = 45 to 65%).
- The enhanced specimens experienced less strain of concrete than the unenhanced specimens (i.e. enhancement percentage at 400 KN = 18 to 32%).
- If the bars are poorly installed and are located near the concrete surface in contact with the air, cracks and damage could easily occur.
- The lifespan of coastal structures most probably would be extended if the steel bars are properly located away of the concrete surface or protected by CFRP sheets.
- It is better to implement CFRP sheets as an enhancement measure ((i.e. enhancement percentage at 400 KN = 23 to 65%).

Based on the achieved experiments, recommendations were prolonged. The extended recommendations are presented here, as follows:

- As for the coastal engineering practice, one should mention that:

- ✓ Bars should be properly installed and should be located away from the concrete surface in contact with the air in order to ensure damage delay.
- ✓ Measures should be undertaken while constructing any coastal structure.
- ✓ Among these measures are increasing the concrete cover to protect the reinforcing steel or adding CFRP sheets to safeguard the steel bars.
- Regarding the coastal engineering research, one should further advise researchers to:
  - ✓ Investigate other measures that could be undertaken during constructing coastal structures (i.e. FRP rebar or FRP).
  - ✓ Inspect these measures to safeguard the steel bars, using different concrete elements (i.e. beams and piles).

## 12. LIST OF REFERENCES

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<b>Specimens Identification</b>	<b>Main (CFRP)</b>	<b>cross section (mm)</b>	<b>Cover (mm)</b>	<b>salts to cement ratio (by weight)</b>	<b>Exposure Period (days)</b>	<b>Type of Specimen</b>
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**Table (1) Designed test program**

1	4 Ø 12 (---)	200 x 200	25	3%	----	Control
S2					180	Unenhanced
S3					365	Unenhanced
S4	4 Ø 12 (---)	200 x 200	25	6%	----	Control
S5					180	Unenhanced
S6					365	Unenhanced
S7	4 Ø 12 (---)	200 x 200	25	10%	----	Control
S8					180	Unenhanced
S9					365	Unenhanced
S10	4 Ø 12 (---)	200 x 200	40	3%	----	Control
S11					180	Enhanced
S12					365	Enhanced
S13	4 Ø 12 (---)	200 x 200	40	6%	----	Control
S14					180	Enhanced
S15					365	Enhanced
S16	4 Ø 12 (---)	200 x 200	40	10%	----	Control
S17					180	Enhanced
S18					365	Enhanced
S19	4 Ø 12 (Sheets)	200 x 200	25	3%		Control
S20						Enhanced
S21						Enhanced
S22	4 Ø 12 (Sheets)	200 x 200	25	6%		Control
S23						Enhanced
S24						Enhanced
S25	4 Ø 12 (Sheets)	200 x 200	25	10%		Control
S26						Enhanced
S27						Enhanced



Photo (1) Implemented cement sacs



Photo (2) Implemented aggregate



Photo (3) Sodium chloride sacs



Photo (4) The laboratory mixer



Photo (5) Wooden formworks



Photo (6) Casting concrete over steel in formworks



Photo (7) Spray wet curing



Photo (8) Loading frame

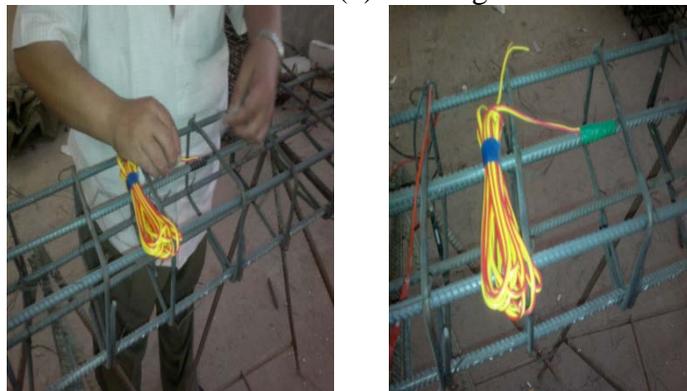
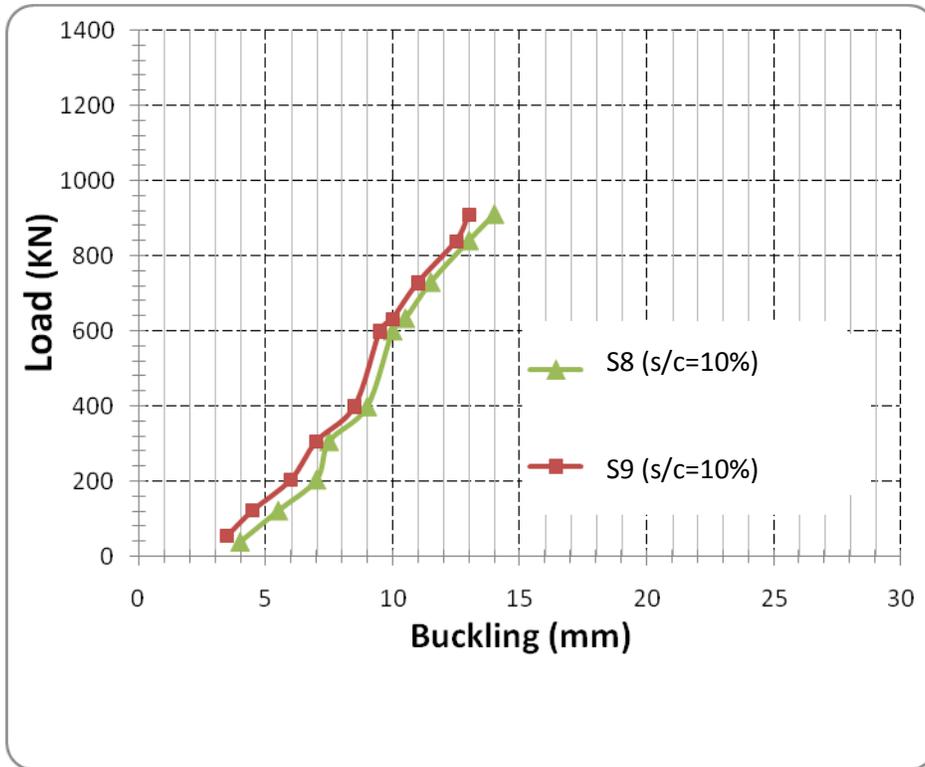


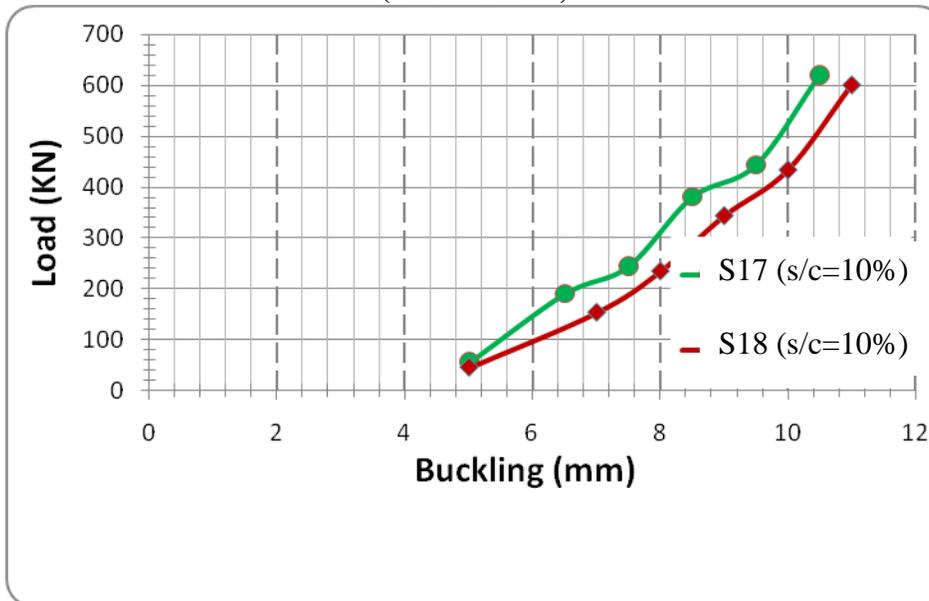
Photo (9) Strain gauges



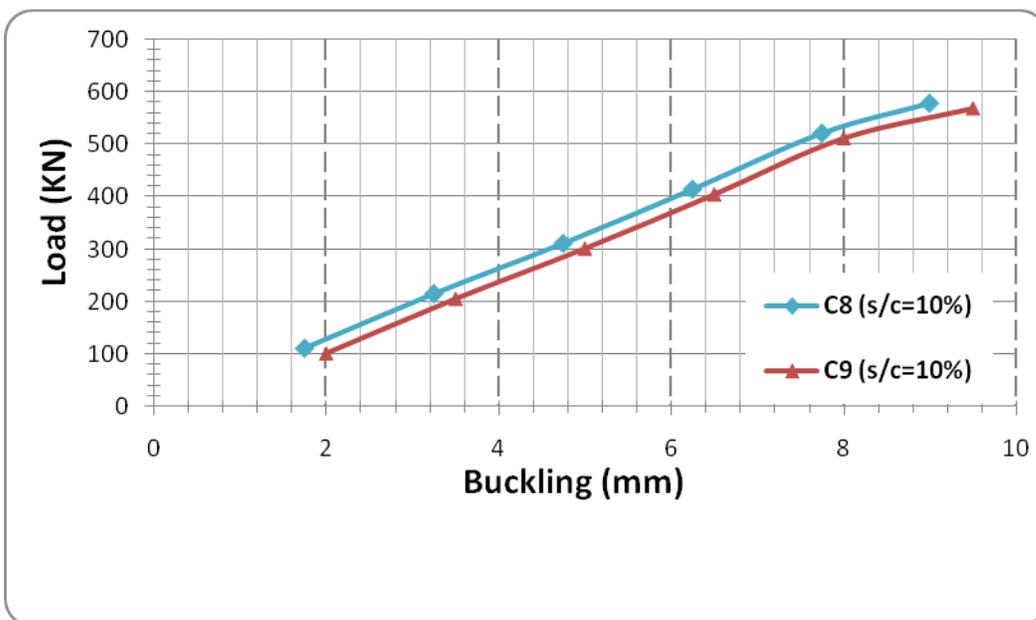
**Photo (10) Specimens during testing**



**Figure (1) Relation between load and buckling (Unenhanced)**



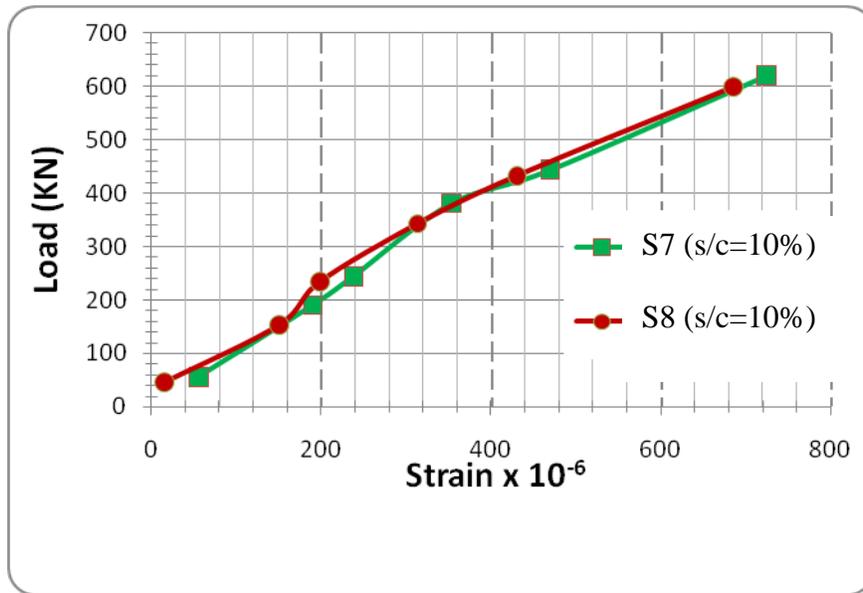
**Figure (2) Relation between load and buckling (Enhanced specimens with 40 mm cover)**



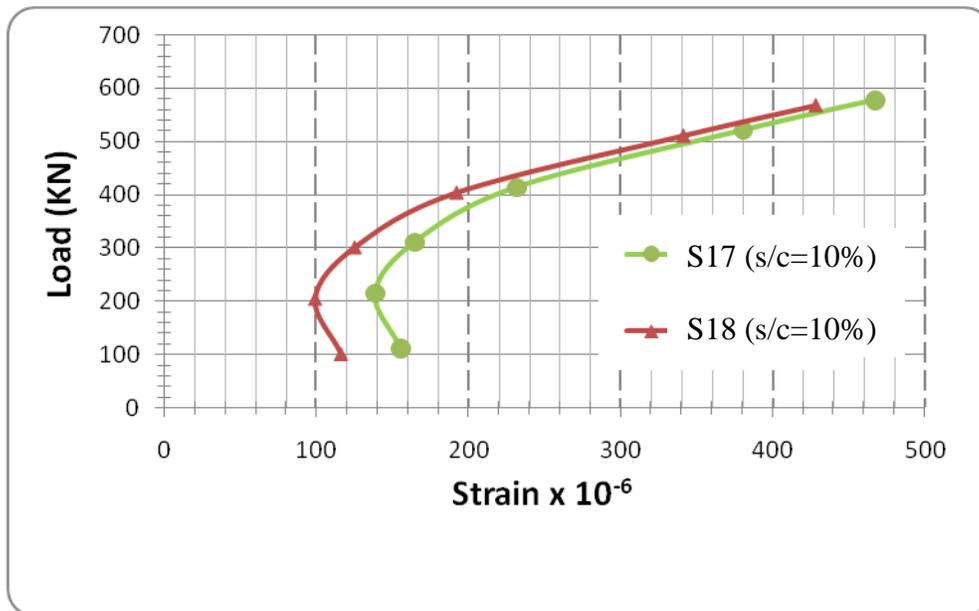
**Figure (3) Relation between load and buckling  
(Enhanced specimens with CFRP)**

S26 (s/c=10%)

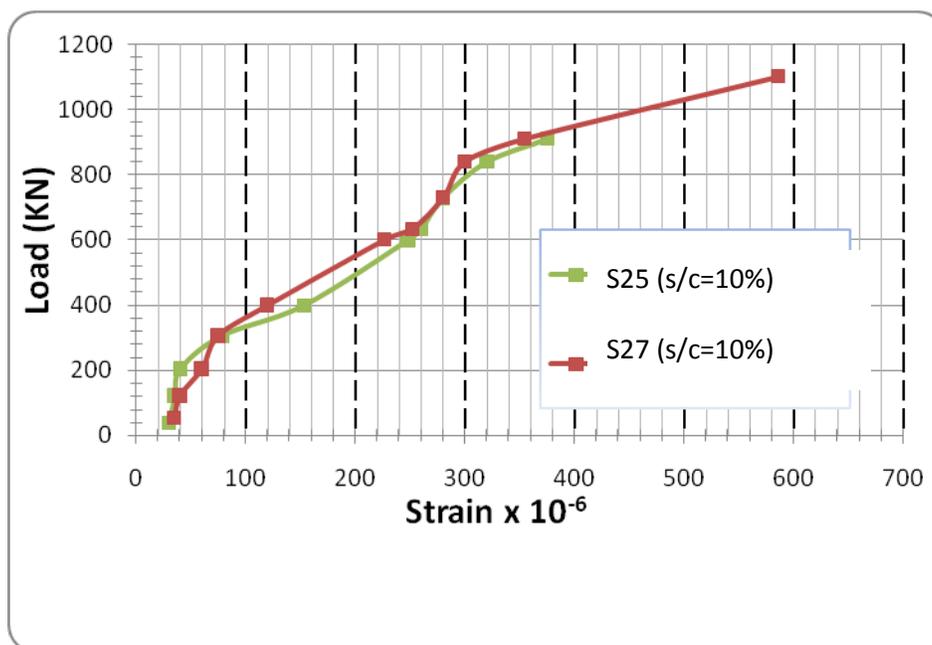
S27 (s/c=10%)



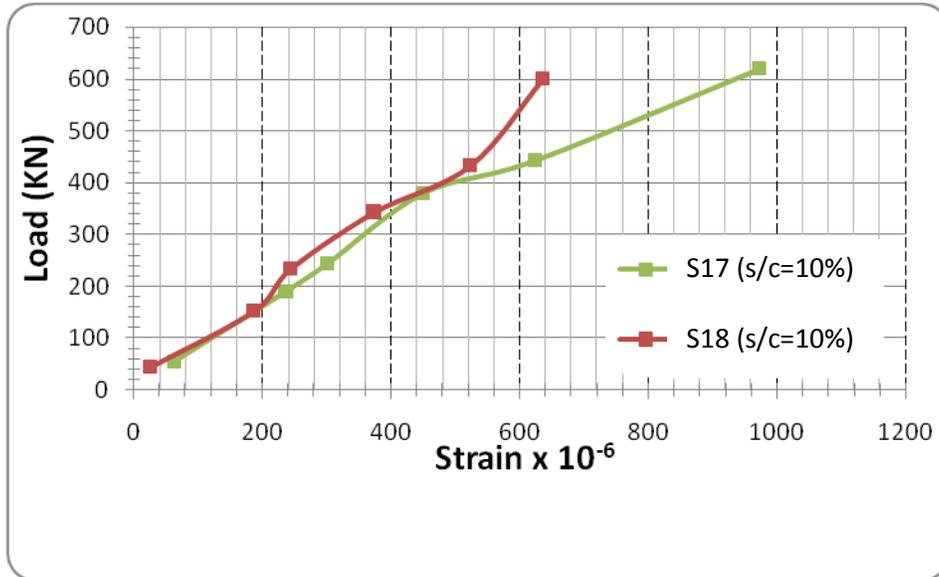
**Figure (4) Relation between load and strain of steel (Unenhanced specimens)**



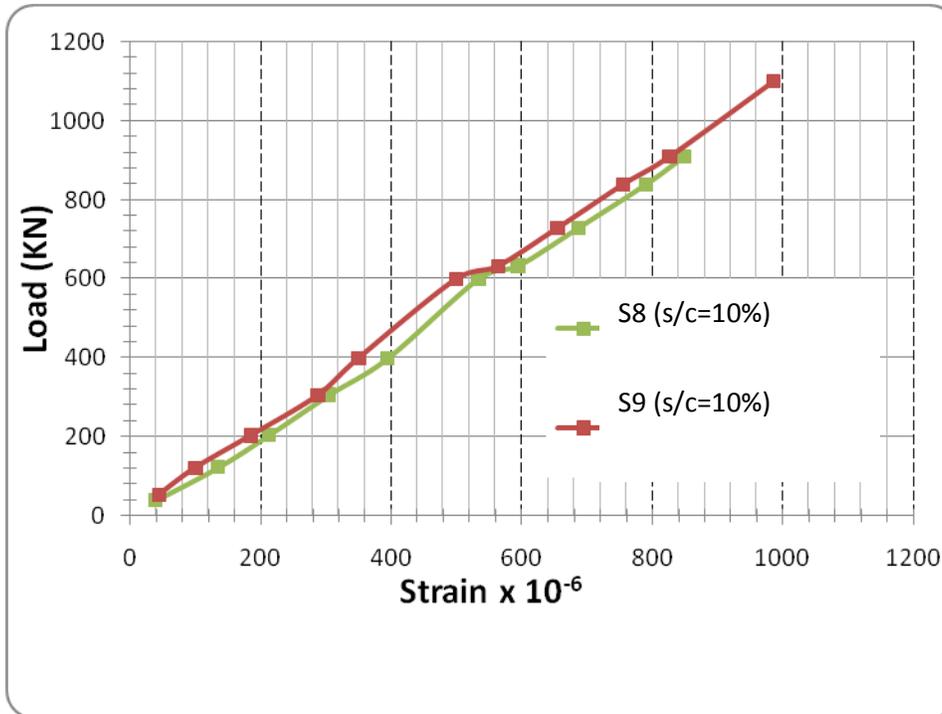
**Figure (5) Relation between load and strain of steel (Enhanced specimens with 40 mm cover)**



**Figure (6) Relation between load and strain of steel  
(Enhanced with CFRP sheets)**



**Figure (7) Relation between load and strain of concrete (Unenhanced)**



**Figure (8) Relation between load and strain of concrete (Enhanced with 40 mm cover)**

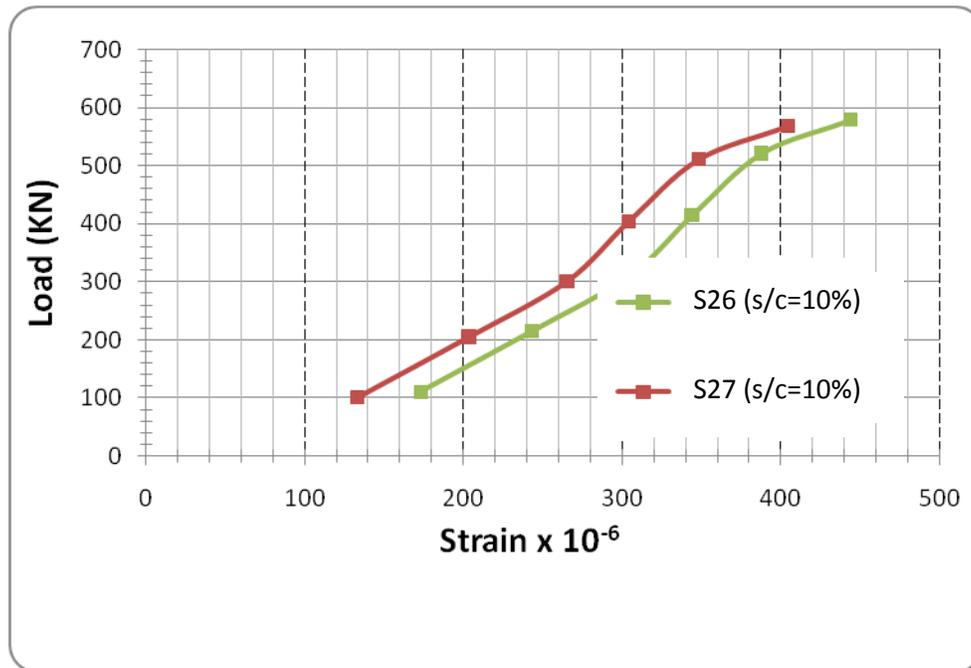


Figure (9) Relation between load and strain of concrete (Enhanced specimens with CFRP)

Table (2) Values of buckling, strain of steel and strain of concrete of the unenhanced specimens, enhanced together with the enhancement percentages

Specimen type / Property	Unenhanced	Enhanced with 40 mm cover	Enhanced with CFRP sheets
Buckling (mm)	9.6	8.4	6.0
Enhancement (%)	--	12.5	37
Strain of steel x10 <sup>-6</sup> mm	440	200	160
Enhancement (%)	--	54	63
Strain of concrete x10 <sup>-6</sup> mm	360	320	300
Enhancement (%)	--	11	16



**Photo (11) Mode of Failure for one of the unenhanced specimens**



**Photo (12) Mode of Failure for one of the enhanced specimens)**