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PERFORMANCE OF LOW EARTH ORBIT SATELLITE SYSTEMS WITH A GAUSSIAN MIXTURES TRAFFIC DISTRIBUTION

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ABSTRACT

A new traffic model for Low Earth Orbit (LEO) Satellite system is proposed. Two different cases are considered. The first case represents the situation in which the traffic load follows a bimodal contaminated Gaussian distribution. The second case considers the trimodal distribution. The parameters of this new distribution model are introduced and their effects on the Signal to Interference Ratio (SIR) and the capacity are investigated.

KEYWORDS

Low Earth Orbit Satellite Communication

I. INTRODUCTION

Low earth orbit satellite communication systems are one of the most appropriate systems to offer personal communications (PC) [1-3]. They can also provide additional advantages for the global communication networks, e.g., small propagation delay and loss, and high elevation angle in high latitude [4].

One of the most recent candidates for establishing the multiple access in LEO satellite systems is Code Division Multiple Access (CDMA). CDMA has higher capacity than TDMA and FDMA if voice activity and frequency reuse by spatial isolation are employed [5]. The non-uniform distribution of the traffic is a normal feature of our globe. However there are only few studies on the effect of this non-uniformity of the traffic on the performance of LEO systems. Performance analysis of

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LEO satellite communication systems with traffic non-uniformity was considered by Abbas, et al., [6]. In his analysis, the traffic model was assumed to have a Gaussian probability density function with variance ω^2 , which represents the traffic non-uniformity. The model represents the case of an isolated city. Due to the relative large area coverage of a LEO satellite, more than one inhabited area can exist in the coverage area of three consecutive satellites. In this case the Gaussian distribution will not be a good choice to represent the traffic non-uniformity. A (rather) more suitable distribution for a lot of practical cases is the Gaussian mixtures, which is considered in this paper.

This paper suggests a general traffic model that can resemble specific areas in the globe. It also discusses the effects of traffic non-uniformity on the performance of the LEO satellite communication system employing CDMA scheme. In section II we define the new traffic model. Section III contains the performance measure (SIR) for three adjacent satellites. Section IV contains the other performance measure namely the capacity for these three adjacent satellites. Section V shows the numerical results. Section VI includes the conclusions.

II. TRAFFIC NON-UNIFORMITY IN LEO SATELLITE SYSTEMS

In this section we cosider the distribution of the traffic in the area covered by the three satellites. In LEO satellite systems, the satellites are organized on a multiple orbit configuration. In the GlobalStar system for example the 48 satellites are organized in 8 orbits, each with 6 satellites

In this model shown in Fig.1, an arc represents an area on the earth [7]. The figure shows the coverage and interference areas of each satellite. The coverage area is specified by the minimum elevation angle (θ_{min}). The interference area of a satellite is specified by the final line of sight of that satellite. An area covered by two satellites will be denoted by "double coverage area" β represents the position of the ith satellite measured from the center of the earth

The Contaminated Gaussian Traffic Model

To analyze the effect of traffic non-uniformity, we define the traffic distribution as:

$$P(\alpha) = A \sum_{i=-M}^{M} \frac{\varepsilon_{i}}{\omega_{i}} \exp\left(\frac{-\left(\alpha - \mu_{i}\right)^{2}}{2\omega_{i}^{2}}\right) \qquad |\alpha| < \pi$$
(1)

where α is the angular distance of any user from the origin measured by the angle at the center of the earth in radians, μ_i is the center of the i^{th} populated area, ω_i is the nonuniformity parameter of the i^{th} populated area and ϵ_i is the weight of the i^{th} populated area relative to the total traffic load. The number of populated areas will depend on "M" and the values of ϵ_i as will be shown later. The constant A is given by:

$$A = B \begin{bmatrix} \frac{3\pi / N S}{\int} & \sum_{i=-M}^{M} \frac{\mathcal{E}_{i}}{\omega_{i}} \exp\left[\frac{-(\alpha - \mu_{i})^{2}}{2\omega_{i}^{2}}\right] d\alpha \end{bmatrix}^{-1}$$
(2)

where B is the total traffic load for the three satellites between $-3\pi/N_s < \alpha < 3\pi/N_s$, N_s, is the number of satellites in one orbit. For the sake of simplicity we will assume that $\omega_i = \omega$ for all i. Next, we shall consider two cases of interest, in particular, the cases of two and three populated areas respectively.

The Case Of Two Populated Areas

In this case, we put in (1), M=1, $\begin{aligned} \epsilon_{-1} &= \epsilon, \qquad \epsilon_0 = 0, \qquad \epsilon_1 = 1-\epsilon, \end{aligned}$ μ_1 = -μ $\mu_1 = \mu_1$ Thus, we obtain the conventional contaminated Gaussian distribution given by:

$$P(\alpha) = \frac{A}{\omega} \left[\varepsilon \exp\left[\frac{-(\alpha + \mu)^2}{2\omega^2}\right] + (1 - \varepsilon) \exp\left[\frac{-(\alpha - \mu)^2}{2\omega^2}\right] \right]$$
(3)

The probability density function (p.d.f.) of (3) is shown in Fig.2.

The Case Of Three Populated Areas

In this case P (a) is given by:

$$P(\alpha) = \frac{A}{\omega} \left[\varepsilon_1 \exp\left[\frac{-(\alpha - \mu)^2}{2\omega^2}\right] + \varepsilon_2 \exp\left[\frac{-\alpha^2}{2\omega^2}\right] + \varepsilon_3 \exp\left[\frac{-(\alpha + \mu)^2}{2\omega^2}\right] \right]$$
(4)

Which is obtained by substituting in (1), $\mu_0 = 0$, $\mu_1 = \mu$ and $\mu_{-1} = -\mu$. ϵ_1 , ϵ_2 and ϵ_3 are the weights of these populated areas and can take any arbitrary values satisfying that $\varepsilon_1 + \varepsilon_2 + \varepsilon_3 = 1$. The p.d.f. of (4) is depicted in Fig.3.

III. EVALUATION OF SIGNAL TO INTERFERENCE RATIO (SIR)

Consider three adjacent satellites. The 1st and 3rd satellites have β_1 , β_3 equal to -2π /Ns, 2π /Ns respectively, while β_2 =0. The received power of satellite i from any user within its service area is Si. Furthermore equal service areas and perfect power control are assumed [6]. Any satellite will be affected by the interference comming from all users in the satellite interference area. Users are assumed to have omni directional antennas. So, the interference of the 1st satellite is given by:

$$\begin{aligned} I_{1} &= S_{1} \int_{-3\pi/N_{*}}^{-\pi/N_{*}} P(\alpha) \quad d \alpha \\ &+ S_{2} \int_{-2\pi/N_{*}}^{-3\pi/N_{*}} P(\alpha) \frac{\left[R + h - R\cos(4\pi/N_{*} + \alpha)\right]^{2} + R^{2}\sin^{2}(4\pi/N_{*} + \alpha)}{\left[R + h - R\cos(2\pi/N_{*} + \alpha)\right]^{2} + R^{2}\sin^{2}(2\pi/N_{*} + \alpha)} \quad d\alpha \end{aligned}$$
(5)
$$&+ S_{2} \int_{-\pi/N_{*}}^{-2\pi/N_{*}} \frac{\left[R + h - R\cos(\alpha)\right]^{2} + R^{2}\sin^{2}(\alpha)}{\left[R + h - R\cos(2\pi/N_{*} + \alpha)\right]^{2} + R^{2}\sin^{2}(2\pi/N_{*} + \alpha)} \quad d\alpha \end{aligned}$$

Similarly the interference of the 2nd satellite can be written as follows:

$$I_{2} = S_{2} \int_{-3\pi/N_{s}}^{-\pi/N_{s}} P(\alpha) d\alpha$$

$$+ S_{1} \int_{-\beta_{l}}^{-\pi/N_{s}} P(\alpha) \frac{\left[R + h - R\cos(2\pi/N_{s} + \alpha)\right]^{2} + R^{2}\sin^{2}(2\pi/N_{s} + \alpha)}{\left[R + h - R\cos(\alpha)\right]^{2} + R^{2}\sin^{2}(\alpha)} d\alpha \quad (6)$$

$$+ S_{3} \int_{\pi/N_{s}}^{\beta_{l}} P(\alpha) \frac{\left[R + h - R\cos(2\pi/N_{s} - \alpha)\right]^{2} + R^{2}\sin^{2}(2\pi/N_{s} - \alpha)}{\left[R + h - R\cos(\alpha)\right]^{2} + R^{2}\sin^{2}(\alpha)} d\alpha$$

Finally the interference of the 3rd satellite is given by:

$$I_{3} = S_{3} \int_{\pi/N_{s}}^{3\pi/N_{s}} P(\alpha) d\alpha$$

$$+ S_{2} \int_{2\pi/N_{s}-\beta_{I}}^{\pi/N_{s}} P(\alpha) \frac{[R+h-R\cos(\alpha)]^{2} + R^{2}\sin^{2}(\alpha)}{[R+h-R\cos(2\pi/N_{s}-\alpha)]^{2} + R^{2}\sin^{2}(2\pi/N_{s}-\alpha)} d\alpha \quad (7)$$

$$+ S_{4} \int_{3\pi/N_{s}}^{2\pi/N_{s}+\beta_{I}} \frac{[R+h-R\cos(4\pi/N_{s}-\alpha)]^{2} + R^{2}\sin^{2}(4\pi/N_{s}-\alpha)}{[R+h-R\cos(2\pi/N_{s}-\alpha)]^{2} + R^{2}\sin^{2}(2\pi/N_{s}-\alpha)} d\alpha$$

Where the first term in (5), (6), and (7) is the interference from the same satellite by its own users and the second and third terms are from users of both adjacent satellites [8-10]. Finally the ith SIR is (S_i/I_i).

IV. CAPACITY MEASUREMENT

Another performance measure in LEO satellite is the system capacity. To find the equation for the capacity, we first determine the ratio of the bit energy-to-noise density for the ith satellite [6]:

$$(E_b / N_0)_i = \frac{BW / R_b}{(I_i / S_i) + (\eta / S_i)}$$
(8)

Where the numerator is the ratio of the total bandwidth (*BW*), to the information bit rate (R_b), and the denominator is the total interference-to-signal ratio plus the ratio of background noise (η), to signal. The thermal noise is assumed Gaussian with zero mean, and variance (η). *I*_i is the total interference reaching the ith satellite, (for i = 1, 2, 3) as given by (5), (6), and (7), and is proportional to the total traffic load, *B*. Therefore the maximum amount of traffic that the system can support for a given condition can be denoted as:

$$B_{I} = \frac{I_{I}}{[I_{I}]_{B=1}}$$
(9)

Where $[I_i]_{B=1}$ means the interference, I_i calculated at B=1. Solving (8) for I_i and substituting it in (9) we have

$$B_{i} = \left(\frac{BW / R_{b}}{(E_{b} / N_{0})_{i}} - \frac{\eta}{S_{i}}\right) \cdot \frac{S_{i}}{[I_{i}]_{B=1}}$$
(10)

From this equation, we can derive the maximum traffic B_i (capacity) for a certain E_b/N_0 on the ith satellite for a, R_b , η given BW, and S_i . Capacity of the satellites (SAT₁, SAT₂ and SAT₃) are calculated, and shown in Figures (8) to (11) for different parameter values.

V. NUMERICAL RESULTS

The SIR and the capacity are calculated for the three consecutive satellites SAT₁, SAT₂ and SAT₃ for the case of two populated areas and three populated areas assuming that all received satellites power are equal. In each case we study the effect of two parameters namely the mean and the weight of the ith populated area (μ , ϵ). For the sake of illustration it is important to mention that the service areas of SAT₁, SAT₂ and SAT₃ extends from (-0.86 rad to -0.29 rad), (-0.29 rad to 0.29 rad) and (0.29 rad to 0.86 rad) respectively.

The effect of the weighting parameter for the 1st case is shown in Fig.4. It is a plot of the SIR of the satellites for $\mu = \gamma/2$, ($\gamma = 2\pi / N_s$) and for two different values of ϵ . SAT₁ and SAT₃ have the same SIR for $\epsilon = 0.5$ since the distribution of the users is the same for both satellites which can be deduced from Fig.2 where the number of users under SAT₁ = SAT₃ = 25 while the number of users under SAT₂ = 50. However, for $\epsilon = 0.1$ there is large unbalance between SAT₁ and SAT₃ where the number of users

under SAT₁ = 45 while number of users under SAT₃ = 5. Therefore SAT₁ and SAT₂ can be considered as a Dense Traffic Satellite (DTS) while SAT₃ as Sparse Traffic Satellites (STS). Furthermore, the SIR for the 2nd satellite changes slightly with the variation of ε because the number of users in its service area is almost the same (~ 50).

The effect of varying μ , for ϵ = 0.5 is shown in Fig.5. As μ approaches 0, the traffic model approaches that of one populated area under the satellite SAT₂. Thus the discrepancy in SIR between the satellites increases, then SAT₂ is DTS and SAT₁ and SAT₃ are STS's.

The performance in case of three populated areas is shown in Figures (6) and (7). Fig.6 shows the SIR of SAT₁, SAT₂ and SAT₃ for $\varepsilon_1 = \varepsilon_3 = 0.1$ and $\varepsilon_2 = 0.8$, as μ changes from $\gamma/3$ to $2\gamma/3$. For such a low weight of ε_1 and ε_3 , we will have SAT₁ and SAT₃ as STS's and SAT₂ as DTS. Fig.7 shows the effect of μ for $\varepsilon_1 = \varepsilon_3 = 0.4$ and $\varepsilon_2 = 0.2$. It is clear that the effect of μ is more pronounced for these values of ε . With the relatively higher values of μ , the three satellites become more balanced (i.e, the discrepancy between DTS, STS is smaller). The unbalance increases as μ decreases.

Notice that results of the case of Gaussian distribution traffic [2] is included in our analysis for $\mu = 0$.

Figures (8) to (11) present the effect of μ_i , ϵ_i on the capacity of the system. In these Figures, BW = 1.25 MHz, Rb = 8 Kb/s, S_i / η = -1dB, and Eb/N0 is greater than 5 dB. Since the capacity is proportional to the SIR when B = 1, the results of the capacity confirm those of the SIR.

VI. CONCLUSIONS

A Gaussian mixture traffic model was introduced, it was shown that this distribution can fit specific cases of the globe, by the proper choice of the parameters ε_i , μ_i and ω_i for all i. Previous models are considered as special cases of this suggested model. We can conclude that varying ε , μ , controls mainly the number of users in each service area thus affects the performance of each satellite. The three adjacent satellites will be balanced if this number is the same for all of these satellites. Otherwise there will be an unbalance between the three satellites resulting in having STS, and DTS. It was shown that the SIR increases from 7 to 16 dB depending on the chosen distribution parameters.

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Fig.3. The distribution of the users in case of three populated areas







Measure of Uniformity in Traffic

Fig.5. SIR in case of two populated areas as a function of traffic nonuniformity for ϵ = 0.5, different values of μ

- e - M







Fig.7. SIR in case of three populated areas as a function of traffic nonuniformity for different values of μ







Fig.9. Capacity in case of two populated areas as a function of traffic nonuniformity for ϵ = 0.5, different values of μ







Fig.11. Capacity for three populated areas as a function of traffic nonuniformity for different values of μ