Dimensional Temperature Distribution Resulting From Propagation of A Light Beam Through an Amplifying Medium

M. M. El-Nicklawy, A. F. Hassan, El. M. A. Nasr, A.A. Hemida, S. L. Diab & S. M. El-Genedy

Helwan University, Faculty of Science, Physics Department

Using the Green function theory, the time dependence of the two dimensional temperature distribution resulting from the volume absorption of a pump beam incident in radial direction and an amplified laser radiation incident in axial direction was analytically determined. The mathematical derivation accounts for the effect of self-focusing generated from the laser beam. As an example computation was carried out on Ruby rod subjected to different pump configurations and laser cross-sections.

1. Introduction:

After the invention of high power lasers a lot of nonlinear effects was discovered as frequency doubling, bistability, three and four wave mixing, parametric amplification etc. One of these effects is the effect of self-focusing which may affect the temperature distribution in the irradiated target and it does significantly modify the prediction of theoretical analysis that leaves out selffocusing. Different authors [1-14] have studded the temperature distribution neglecting the effect of self-focusing generated in an irradiated target. This work is devoted to study the time dependent temperature distribution in two dimensions generated from the pump process and the absorption of the amplified radiation incident in axial direction in a rod placed in the focal axis of a cylinder having an elliptical cross-section. The pump source was mounted in the other focal axis. The radiation of the laser beam was considered to initiate self-focusing during its propagation in the rod. The incident laser radiation was considered to have different radii. The pump configuration was assumed to allow for different radial profile of the inverted atoms. This capability plays an important role in:

- 1- The energy consumption of the pump source.
- 2- The life time of the pump source.
- 3- The pump efficiency.
- 4- The heat generated from the pump source.

- 5- The radial amplification of the incident laser beam after being amplified.
- 6- The heat generated from the laser beam into the radial and the axial direction of the rod.

2. Theory

Assuming that a homogeneous isotropic cylindrical shaped target with circular cross-section was illuminated in axial direction with a laser beam and that the target can amplify the laser radiation. Due to this assumption the target was pumped radially with a radiation originating from a gas discharge tube located in the focal axis of a cylinder with elliptical cross-section having reflecting surface. The target was placed in the other focal axis where the pump radiation was differently focused. The laser beam, which has a maximum temporally coinciding with that of the pump pulse, was considered to have the same temporal profile but with different pulse duration. Its spatial distribution was considered to have either a Gaussian shape of different constant or increasing cross-section along the propagation direction (Gaussian beam). Moreover it is assumed that a part of the pump radiation and that of the amplified laser were absorbed during their propagation within the target which was cooled radially at the outer cylinder surface.

Considering no plasma formation at the irradiated surface, and negligible multiphoton absorption the equations governing the temperature distribution are given by:

1) The heat generation equations in cylindrical coordinates

i- Originating from the pump beam

$$\frac{\partial^2 T_p(r,t)}{\partial r^2} + \frac{1}{r} \frac{\partial T_p(r,t)}{\partial r} + \frac{1}{k} g_p(r,t) = \frac{1}{\alpha} \frac{\partial T_p(r,t)}{\partial t}$$
(1)

ii- Originating from the laser radiation

$$\frac{\partial^2 T_L(r,z,t)}{\partial r^2} + \frac{1}{r} \frac{\partial T_L(r,z,t)}{\partial r} + \frac{\partial^2 T_L(r,z,t)}{\partial z^2} + \frac{1}{k} g_L(r,z,t) = \frac{1}{\alpha} \frac{\partial T_L(r,z,t)}{\partial t}$$
(2)

2) The boundary condition describing the cooling at the outer radius of the rod.

$$-k \frac{\partial T_t(r,z,t)}{\partial r}\Big|_{r=R} = h T_t(r,z,t)\Big|_{r=R}$$
(3)
$$\Gamma_t(r,z,t) = T_1(r,z,t) + T_P(r,t)$$
(4)

With $T_t(r,z,t) = T_L(r,z,t) + T_P(r,t)$

where

- T_P (r,t) is the temperature distribution generated from the absorbed pump radiation;
- T_L (r,z,t) is the temperature distribution generated form the absorbed part of the amplified laser beam;

k is the thermal conductivity of the material; $\alpha = \frac{k}{\rho C_P}$ is the thermal diffusivity

of the material, ρ is the mass density of the material; C_P is the specific heat of the medium by constant pressure; g_p (r,t) is the rate of energy generated from the absorbed part of the pump beam per unit volume; g_L(r,z,t) is the rate of energy generated from the absorbed part of the amplified laser beam per unit volume and h is the heat transfer coefficient.

The temperature distribution $T_{P}(r,t)$ resulting from the pump beam was found through the determination of the Green function $G_{p}(r,t|r',\tau)$

$$T_{p}(r,t) = \frac{\alpha}{k} \int_{\tau=0}^{t} d\tau \int_{R} r' G_{p}(r,t | r',\tau) g_{p}(r',\tau) dr'$$
(5)

with

$$G_{p}(r,t | r',\tau) = \sum_{m=1}^{\infty} e^{-\alpha\beta_{m}^{2}(t-\tau)} \frac{1}{N(\beta_{m})} J_{o}(\beta_{m}r) J_{o}(\beta_{m}r')$$
(6)

 β_m are the positive roots of the equation $\beta_m J'_o(\beta_m R) + H J_o(\beta_m R) = 0$

$$N(\beta_m) = \int_0^R r J_o^2(\beta_m r) dr = \left[\frac{2\beta_m^2}{J_o^2(\beta_m R)R^2(H^2 + \beta_m^2)}\right]^{-1}$$
(7)

$$g_{p}(r,t) = X \int_{\nu_{1}}^{\nu_{2}} \alpha(\nu) G_{p}(t) I_{op\nu}(\nu) \frac{R_{o} + R}{R_{o} + r} e^{\alpha(\nu)(r-R)} d\nu$$
(8)

and

$$G_{p}(t) = \frac{(n+1)^{(n+1)}}{n^{n}} \frac{t}{\Delta t_{p}} (1 - \frac{t}{\Delta t_{p}})^{n} \qquad n = 3 \quad 0 \le t \le \Delta t_{p} \qquad [15, 16] \qquad (9)$$

with H=h/k, $J_o(\beta_m r)$ and $J'_o(\beta_m R)$ are the Bessel functions of zero order and first order respectively, $G_p(t)$ is the time profile of the pump beam, Δt_p is the pulse duration of the pump beam.

The temperature distribution resulting from the laser radiation is given by

$$T_{L}(r,z,t) = \frac{\alpha . 2\pi}{k} \int_{r=0}^{R} \int_{\tau=0}^{t} r' \sum_{m=0}^{\infty} \frac{2\beta_{m}^{2}}{R^{2}(H^{2} + \beta_{m}^{2})} \frac{1}{J_{o}^{2}(\beta_{m}R)} \exp\left[-\alpha\beta_{m}^{2}(t-\tau)\right]$$
$$J_{o}(\beta_{m}r')J_{o}(\beta_{m}r)\int_{o}^{L} G_{L}(z,t|z',\tau).g_{L}(r',z',\tau)dr'dz'd\tau$$
(10)

with

$$G_{L}(z,t|z',\tau) = \frac{1}{2\sqrt{\alpha}\sqrt{\pi}\sqrt{t-\tau}} \left[\exp\left[\left(\frac{2L-z-z'}{2\sqrt{\alpha}}\right)^{2}\frac{1}{t-\tau}\right] + \exp\left[\left(\frac{z+z'}{2\sqrt{\alpha}}\right)^{2}\frac{1}{t-\tau}\right] + \exp\left[\left(\frac{2L-z+z'}{2\sqrt{\alpha}}\right)^{2}\frac{1}{t-\tau}\right] + \exp\left[\left(\frac{2L-z-z'}{2\sqrt{\alpha}}\right)^{2}\frac{1}{t-\tau}\right] + \exp\left[\left(\frac{2L-z-z'}{2\sqrt{\alpha}}\right)^{2}\frac{1}{t-\tau}\right] + \exp\left[\left(\frac{4L-z-z'}{2\sqrt{\alpha}}\right)^{2}\frac{1}{t-\tau}\right] + \exp\left[\left(\frac{4L-z-z'}{2\sqrt{\alpha}}\right)^{2}\frac{$$

$$g_{L}(r,z,t) = \int_{\upsilon} I_{oL\upsilon}(\upsilon,r,0,t) \alpha_{h} \exp(-(\alpha_{L}(\upsilon,r,t) - \beta_{L}(\upsilon,r,t))z) d\upsilon \quad (12)$$

$$I_{oLv}(v, r, 0, t) = \tilde{I}_{o}g_{L}(v, v_{oL})g_{L}(r)G_{L}(t)$$
(13)

and

$$G_{L}(t) = \frac{(n+1)^{n+1}}{n^{n}} \frac{(t-\Delta t_{o})}{\Delta t_{L}} (1-(t-\Delta t_{o})/\Delta t_{L})^{n}$$
 [15,16] (14)

where

 $I_{oLv}(v,r,0,t)$ is the spectral intensity distribution of the laser beam incident in axial direction on the pumped laser rod at z=0, $\alpha_{\rm h}$ is the coefficient responsible for the heating process it has according to [7] the value 20 1/m, $\alpha_{\rm L}(v,r,t)$ and $\beta_{\rm L}(v,r,t)$ are the linear attenuation and amplification coefficient of the pumped rod in the frequency region of the incident laser radiation respectively, $\tilde{I_o}$ is the maximum of the incident laser intensity, $g_L(v,v_{oL})$ is the spatial line profile of the laser beam with the central frequency v_{oL} , $G_L(t)$ is the temporal profile of the laser beam, Δt_o is the time retardation for coinciding the maximum of the pump beam with the laser beam, Δt_L is the pulse duration of the laser beam, $g_L(r)$ is the radial distribution of the laser radiation given for the case of Gaussian distribution when self-focusing is not considered by :

$$g_{L}(r) = e^{-\frac{2r}{w_{o}^{2}}}$$
(15)

 $g_L(r,z)$ is the radial distribution of the laser radiation given for the Gaussian distribution and Gaussian beam considering self-focusing by $w^2 = -2\frac{r^2}{r^2}$

$$g_{L}(r,z) = \frac{w_{0}^{2}}{w(z)^{2}} e^{-\frac{2}{w(z)^{2}}}$$
(16)

where w_o is the width of the laser beam at the irradiated surface of the rod at z=0 and w(z) is the width at any location z within the rod, w_o and w(z) in the cases of Gaussian distribution and Gaussian beam have to be determined as follows.

Self focusing is a focusing of a beam, caused by the beam itself through a nonlinear process. In this situation, the higher intensities on the beam axis, as compared to the wings of the spatial intensity distribution, cause an effectively increased <u>refractive index</u> for the inner part of the beam. This modified refractive index distribution then acts like a focusing lens. As the beam radius is reduced, the optical intensities become even higher, leading to further increase of the self-focusing. This mechanism can lead to very high optical intensities which can easily destroy the optical medium.

The nonlinear refractive index of a medium is given by [17]

$$n = n_0 + n_2 E^2$$
 with $E = \frac{1}{2} (\hat{E}(\omega) e^{-i\omega t} + cc)$ (17)

where E is the electric field amplitude of the light beam n_2 is a material constant and n_o is the refractive index when the field is very week. The dependence of the beam width on the distance covered by the beam in a medium can be obtained from Maxwell's equation. The wave equation of the electric field when the square of the refractive index given by equation (17) is approximated for $n_0 >> n_2$ by $n^2 \approx n_0^2 + 2n_0n_2E^2$ can be written as[17]:

$$\nabla^2 E - \frac{n^2}{c^2} \frac{\partial^2 E}{\partial t^2} \approx \nabla^2 E - \frac{1}{c^2} (n_0^2 + 2n_0 n_2 E^2) \frac{\partial^2 E}{\partial t^2} = 0$$
(18)

Equation (18) becomes in paraxial approximation after averaging over an optical period[17]

$$\nabla_T^2 \hat{E} + 2ik \, \frac{d\hat{E}}{dz} + \frac{k^2 n_2}{n_o} \left| \hat{E} \right|^2 \hat{E} = 0 \tag{19}$$

where ∇_T^{2} is the transverse Laplacian

Since the dependence of the width w on z is required equation (19) has to be solved.

Assuming the solution of equation (19) to be given by

$$\hat{E}(\vec{r}) = A(\vec{r})e^{iks(r)}$$
⁽²⁰⁾

where A and S are real functions. Equation (20) and (19) give

$$\frac{\partial A^2}{\partial z} + \nabla_T \cdot (A^2 \nabla_T s) = 0$$
⁽²¹⁾

and

$$2\frac{\partial s}{\partial z} + \left(\nabla_T s\right)^2 = \frac{\nabla_T^2 A}{k^2 A} + \frac{n_2 A^2}{n_0}$$
(22)

Assuming $\vec{A(r)}$ to be represented by a Gaussian beam given by

$$A(\vec{r}) = \frac{A_0 w_0}{w(z)} e^{-r^2 / w^2(z)}$$
(23)

One gets after some mathematical manipulation the following equation[17].

$$w(z) = w_0 \left[1 - \left(\frac{P_0}{P_{cr}} - 1\right) \frac{z^2}{z_0^2}\right]^{1/2}$$
(24)

with P₀ is the incident power

$$z_0 = \frac{kw_0^2}{2}$$
 and $P_{cr} = c\varepsilon_0 \lambda^2 / 8\pi n_2$

It is worth noting that equation (24) tends to that of a Gaussian beam as $P_{\rm o}$ tends to zero.

Equation (24) is valid for the case where transformation of the beam parameter resulting from its propagation through different media is not considered. Considering the transformation of w_0 [17] after passing a free space of thickness d and refractive index n_{01} and refracted by a medium of refractive index n_{02} , w(z) will be written after replacing w_0 by w(z=0) given from the linear case (part I) by equation $w(z=0) = \sqrt{\frac{\lambda \tilde{L}}{2\pi n_{01}}} \sqrt{1 + \frac{(n_{02}\tilde{L} + 2n_{02}d)^2}{n_{02}^2\tilde{L}^2}}$ (25)

where \tilde{L} is the resonator length equal to the rod inside it. Thus w(z) can be written as

$$w(z) = \sqrt{\frac{\lambda \tilde{L}}{2\pi n_{01}}} \sqrt{1 + \frac{(n_{02}\tilde{L} + 2n_{02}d)^2}{n_{02}^2\tilde{L}^2}} [1 - (\frac{p_o}{p_{cr}} - 1)\frac{z^2}{z_o^2}]^{1/2}$$
(26)

Setting w(z) given by equation (26) in equation (16) one gets the radial distribution of the Gaussian beam case of self-focusing.

Since a Gaussian distributed laser radiation does not change its width along its propagation direction z as self-focusing is not considered, thus w(z) can be given by

$$w(z) = w_0 \left(1 - \frac{p_o}{p_{cr}} \frac{z^2}{z_0^2}\right)^{1/2}$$
(27),

and the radial distribution given by equation (16) will be written as

$$g_{L}(r,z) = \frac{w_{0}^{2}}{w(z)^{2}}e^{-2\frac{r^{2}}{w(z)^{2}}}$$

3. Computation:

Calculation of the temperature resulting from the absorbed laser beam $T_L(r, z, t)$:

Since this work deals with medium having $(\beta_L - \alpha_L) \neq 0$, the medium was subdivided into equal spaced intervals $\Delta z = L/m$. The input power of each interval was assumed to be

$$P_o e^{(\beta_L - \alpha_L)N\,\Delta z} \tag{28}$$

where N takes values from N=0 to m. w_o of the radial distribution given by equation (16) was considered at the beginning of each interval to be that calculated from w(z) at the end of the previous interval. The power within the interval was considered to be constant.

To get $T_L(r, z, t)$ equation (10) was calculated after substituting for $G_L(z, t | z', \tau)$, $g_L(r', z', \tau)$ and $G_L(t)$ from equations (11),(12) and (14) respectively. For the case of Gaussian beam the radial intensity distribution of the laser radiation was considered to be given by equation (16), after replacing w_0 and w(z) from equations (25) and (26) respectively. For the case of Gaussian distributed laser radiation the radial distribution is given by equation (16) but with w_0 = constant and w(z) given by equation (27).

The computation was carried out considering $w_o = 10^{-4}$ m for the Gaussian distribution and $w_o = 1.77 \times 10^{-4}$ m at z=0 for the Gaussian beam and a maximum monochromatic laser intensity $\tilde{I_o}$ given by $\tilde{I_o} = 10^{11}W / m^2$ at r=0 and $t = \Delta t_p / 4$.

The locations and the times at which the temperature was calculated are the multiple of the following Δz , Δr_i and Δt_i values

 Δz is considered to be given by $\Delta z = L/10$

 Δr_i values are given according to the following table

The radius of the rod R was according to the width of the laser beam and R_o values subdivided into three zones Δr_i

$\Delta r_1 = R_o / 10$	$0 \le r \le R_o$
$\Delta r_2 = (w_o - R_o)/10$	$R_o \prec r \leq w_o \text{ or } w_o \prec r \leq R_o$
$\Delta r_3 = (R - w_0)/10$	$w_{a} \prec r \leq R$

The time was sliced into four different intervals Δt_i .

$$\Delta t_1 = \text{the time before initiating the laser pulse was divided by 5}$$

$$t = \Delta t_1 \times n_1 \qquad n_1 = 0.....5$$

$$\Delta t_2 = \text{the time during the laser pulse duration was divided by 16}$$

$$t = \Delta t_1 \times 5 + \Delta t_L / 16 \times n_2 \qquad n_2 = 1.....16$$

 Δt_3 = the time calculated from the equation (the pump pulse duration – (the time before initiating the laser pulse + pulse duration)) was divided by 5

$$t = (\Delta t_p - (\Delta t_1 \times 5 + \Delta t_L))/5 \times n_3 + (\Delta t_1 \times 5 + \Delta t_L) \qquad n_3 = 1....5$$

the time after switching off the pumping process was given by

 $\Delta t_4 = 2X$ pulse duration of the pump beam

$$t = \Delta t_p + n_4 \times \Delta t_4 \qquad \qquad n_4 = 1 \dots 7$$

Since the integration was carried out over z', r' and τ , $\Delta z, \Delta r_i$ and Δt_i were subdivided into 6,6,5 equal intervals respectively.

Symbol	р kg	C _p	N₀ ions	$\nu_{_{01}}$	v_{21}	$\nu_{_{22}}$	v_{31}	$\nu_{_{32}}$	$F_{\perp}^{\ 21}$	
Unit	$\overline{m^3}$	$\frac{w . \sec}{kg .^{o}k}$	$\overline{m^3}$	Hz	Hz	Hz	Hz	Hz	1/m	
Value	4300	43	1.58E25	1.5E15	7.3E14	7.1E14	5.4E14	5.53E14	320	
Symbol	$F_{\perp}^{\ 31}$	F_{\square}^{32}	$F_{\scriptscriptstyle \square}^{ 01}$	$F_{\scriptscriptstyle \Box}^{22}$	Δv_o	k w	h W	<i>p</i> _{cr}	no	$\frac{\mathbf{n}_2}{m^2}$
Unit	1/m	1/m	1/m	1/m	Hz	$\frac{w}{m^{o}K}$	$\overline{m^{\circ}K}$	W		$\frac{1}{V^2}$
Value	155	285	360	280	0.3298E12	42	10000	5000	1.759	2E-14

Table (1): physical and thermal parameter of Ruby:

 $F_{\Box \perp}^{\ ij}$ is the absorption coefficient parallel and perpendicular to the C –axis of the crystal

 v_{ij} are the corresponding central frequency to F^{ij}

 p_{cr} is the critical power

 N_o is the Cr^{3+} concentration

 n_0 is the average refractive index of \Box and \perp radiation at $\lambda = 6943 \mathring{A}$

 n_2 is the coefficient of the part of the refractive index depending on square of the electric field strength.

4. Results and Discussion:

Figure (1) represents the radial distribution of $(\beta_L - \alpha_L)$ calculated at $t = \Delta t_p / 4$ and R_o as a parameter. The observation of the curves shows that, for $R_o=10^{-4}$ m and 5×10^{-4} m $(\beta_L - \alpha_L)$ in the vicinity of r =0 has a relative minimum shifted towards smaller r values as R_o increases, and that the minimum of the former R_o value is more pronounced than that of the latter one. The curves calculated for $R_o=10^{-3}$ m and ∞ m grow monotonically and exhibit specially for the case $R_o=\infty$ m a saturated behavior at r=R. This behavior can be explained in view of the fact that the behavior $(\beta_L - \alpha_L)$ is dictated from the intensity

distribution of the pump beam given by $\frac{R_0 + R}{R_0 + r}e^{\alpha(r-R)}$ which exhibits a

minimum at $r = \frac{1}{\alpha} - R_0$. Since the value of α is about 10^{-3} m⁻¹ it follows that by

increasing R_o values the position of the minimum will shift towards smaller r values. As R_o is given values greater than or equal to $1/\alpha$ the position of the minimum will shift to such small or negative r values where the relative minimum disappears. Since $(\beta_L - \alpha_L)$ at r = 0 must be 46.05 m⁻¹, this is because an amplification of 100 at z = L is set as a condition, and $(\beta_L - \alpha_L)$ depends on the pump energy density elsewhere, thus a minimum laying to the right of r = 0 can have positive or negative values. In case of strong focusing the intensity of the pump radiation drops strongly with r leading to negative $(\beta_L - \alpha_L)$ values. The saturation at r=R for $R_0 = \infty$ m results from the behavior of $(\beta_L - \alpha_L)$ which is generally according to part I [18] given by

$$(\beta_{l} - \alpha_{l}) = c \frac{c_{1} \frac{R_{0} + R}{R_{0} + r} e^{\alpha(r-R)} - 1}{c_{1} \frac{R_{0} + R}{R_{0} + r} e^{\alpha(r-R)} + 1}$$

Figure (2) represents the axial distribution of the laser beam width calculated for w=10⁻⁴m of the incident laser radiation at $t = \Delta t_p / 4$, r=0. Since the amplification at r=0 is independent of R_o, therefore all the curves of the different R_o values will coincide on each other. The figure shows that the width exhibits a minimum. The appearance of minimum is due to the dependence of P_o on z as given by the equation $w(z) = w_o \left| \left[1 - \frac{P_o(z)}{P_{cr}} \frac{z^2}{z_o^2} \right] \right|^{1/2}$. where $P_o(z)$ is

given by equation (28).



Fig. (1): The radial distribution of the net amplification coefficient of the laser radiation $(\beta_L - \alpha_L)$ calculated at $t = \Delta t_p/4$ with R_o as a parameter. $R_o = 10^{-4}$ m curve A $R_o = 5X10^{-4}$ m curve B $R_o = 10^{-3}$ m curve C $R_o = \infty$ m curve D



Fig. (2): The variation of the width (w) of a laser beam having a Gaussian spatial intensity distribution calculated as a function of z. for $w_0 = 10^{-4}$ m.

Case of Gaussian distribution w=10⁻⁴m:

The temporal temperature distribution calculated at z=0, r=0 and R_o as a parameter, shows that the temperature behaves in relative distribution and absolute value as the corresponding ones of the linear case (part I). This behavior is due to the fact that at z=0, r=0 non of the nonlinear effects has taken place and the effect of locations other than zero is negligible small.

Figure (3) represents the temperature versus time calculated at z=L, r=0 and R_o as a parameter. The curves show that the maximum of the temperature is not at $t = \Delta t_p / 4$ but at greater t value. This behavior is for all R_o values due to the fact that before reaching the temperature its maximum value the accumulation of heat overcompensates the losses. At the maximum temperature the losses are equal to the heat generated. For times greater than the time of maximum temperature the losses are greater than the generated heat. The small slop of the time profile after switching off the laser radiation seen for $R_0=10^{-3}$ m is due to the heat transfer from the maxima surrounding r=0 see Fig. (5) which leads to increase the minimum around r=0 and decrease the heat transfer. The appearance of a minimum followed by a maximum for $R_0 = \infty m$ is due to the heat transfer from r=0 into its surrounding which as seen from Fig. (5) occurs firstly and leads to the minimum temperature. As the time increases the heat conduction from the maximum located at greater r-value will increase the temperature at r=0. This behavior lasts till the heat transfer into the region around r=0 is equal to the heat transfer out of this region where a maximum of the temperature occurs. After attaining the temperature its maximum value, it begins monotonically to decrease with small slop as t increase. That the maximum of the temperature increases with increasing R_o values is due to the increased width of the laser radiation at z=L which, as seen from Fig. (5), leads to increase the interval of the radial distribution of $(\beta_L - \alpha_L)$ contributing to the heating effect. The maximum of the temperature in this case is for R_o=10⁴m and R_o=5X10⁴m smaller than the corresponding ones in the linear case (part I). This behavior is, for both cases, due to the increase of w (L) value which leads to a smaller intensity and it is for R_o=10⁴m due to the negative behavior of the radial distribution of $(\beta_L - \alpha_L)$. For R_o=5X10⁴m it is due to the temperature is higher than the linear case. This is because the increase of w (L) value will cover areas having greater $(\beta_L - \alpha_L)$ values that overcompensate the decrease of the intensity.



Fig. (3): The temporal temperature distribution induced by a laser beam having a Gaussian spatial intensity distribution of width $w_o = 10^{-4}$ m and pulse duration $\Delta t_L = 10^{-4}$ sec calculated considering self-focusing and amplified power at z = L, r = 0 and R_o as a parameter.

 $R_o = 10^{-4}m$ curve A $R_o = 5X10^{-4}m$ curve B $R_o = 10^{-3}m$ curve C $R_o = \infty m$ curve D

Figure (4) represents the temperature distribution along the z axis calculated at $t = \Delta t_n / 4$, r=0 and R_o as a parameter. The case of R_o=10⁻⁴m begins with higher temperature due to the great intensity. With increasing z the temperature decreases. This behavior is due to the negative value of $(\beta_L - \alpha_L)$ in the wings of the laser radiation which is greater than the increase of the intensity due to the reduced value of w(z) and the magnification within small r values. As w (z) becomes closer to the minimum the intensity increases and the temperature becomes maximum. The further increase of z leads to smaller intensity (greater w (z)) and truncation of the laser radiation due to the negative $(\beta_I - \alpha_I)$ values which can not be compensated from the increased amplification $e^{((\beta_L - \alpha_L)z)}$ in the small remaining width of the laser radiation and the temperature decreases. For R_o=5X10⁻⁴m ($\beta_I - \alpha_I$) decreases slowly with increasing r value but still remains positive. This behavior lasts up to r=5X10⁻ ⁴m after which it begins to increase. Since w(z) decreases with increasing z value the temperature increases monotonically. As w(z) takes great value such that the wings of the laser radiation will be amplified and the amplification compensates the decrease of the intensity and other losses, such as cooling and heat conduction, the curve attains a maximum. Further increase of z leads to a greater decrease of the intensity than the increase through the amplification and the temperature decreases with increasing z value. For $R_0=10^{-3}m$ a monotone increase of the temperature is observed. This is due to the increased intensity before the minimum width is achieved which overcompensates the reduced radial amplification of $(\beta_L - \alpha_L)$ and the strong increase of w(z) after the minimum which covers greater radial interval from $(\beta_L - \alpha_L)$ and thus leading to greater amplification than the attenuated intensity. The same behavior is also observed for $R_0 = \infty$ m. Due to the increased value of $(\beta_L - \alpha_L)$ in the wings of the laser radiation as Ro increases the maximum temperature increases with increasing R_o values. Due to the greater width of the laser radiation at z=L than the linear case and the behavior of $(\beta_L - \alpha_L)$ for R_o>10⁻³m the temperature in this case is greater than that in the linear case (part I)

Figure (5) represents the radial temperature distribution calculated at $t = \Delta t_p / 4$, z=L and R_o as a parameter. From the figure it is found that the temperature at r=0 increases with increasing R_o values. This is because of the accumulation effect of the heat over the time which is greatest for great R_o values (higher temperature of the surrounding parts around r=0) and the smaller heat conduction in the surrounding. For R_o $\geq 10^{-3}$ m there are two maxima symmetric to the temperature at r=0. This is due to the increased width of the laser radiation which allows, due to $(\beta_L - \alpha_L)$ behavior, the wings of the laser radiation to be amplified. Since in the linear case, part[I], the value of the laser beam width is constant along the z axis no dip was observed.



Fig. (4): The temperature distribution as a function of z induced by a laser beam having a Gaussian spatial intensity distribution of width $w_o = 10^{-4}$ m and pulse duration $\Delta t_L = 10^{-4}$ sec calculated considering self-focusing amplified power at t $= \Delta t_p/4$, r = 0 and R_o as a parameter.

 $R_0 = 10^{-4}m$ curve A $R_0 = 5X10^{-4}m$ curve B $R_0 = 10^{-3}m$ curve C $R_0 = \infty m$ curve D



Fig. (5): The radial temperature distribution induced by a laser beam having a Gaussian spatial intensity distribution of width $w_o = 10^{-4}$ m and pulse duration $\Delta t_L = 10^{-4}$ sec calculated considering self-focusing amplified power at $t = \Delta t_p/4$, z = L=0.1m and R_o as a parameter.

 $R_o = 10^{-4}m$ curve A $R_o = 5X10^{-4}m$ curve B $R_o = 10^{-3}m$ curve C $R_o = \infty m$ curve D

Case of Gaussian Beam:

Figure (6) represents the axial distribution of the laser beam width w(z) given by equation (24) calculated at $t = \Delta t_p / 4$, r=0. Due to the reasons given in Fig. (2) the curves of different R_o values coincide on each other. This is because the amplification is a function of the radius of the pumped rod and not a function of the type of the laser radiation so far saturation effect is not considered. That the minimum width occurs at greater z value than the case of w_o=10⁻⁴m is due to the greater w_o value which is equal 1.77X10⁻⁴m at z=0 and the increasing w(z) with increasing z value when self-focusing is not considered. Thus due to both effects greater power is needed to get minimum width and this is achieved through the amplification of the laser radiation at greater z value than in case of w_o=10⁻⁴m.



Fig. (6): The variation of the width w of a laser having a Gaussian beam intensity distribution as a function of z calculated considering self-focusing and amplified power.

The temporal temperature distribution calculated at z=0, r=0 and R_o as a parameter, shows that the temperature behaves in relative distribution and absolute value as the corresponding ones of the linear case (Part I).

Figure (7) represents the temporal temperature distribution calculated at z=L, r=0 and R_0 as a parameter. Due to the reasons given previously in case of $w_0=10^{-4}$ m the maximum of the temperature is shifted towards greater t values than $t = \Delta t_p / 4$. The increase of the temperature with increasing R_o values is due to the explanation given in Fig. (3). The slow reduction of the temperature for $R_0 > 5X10^{-4}$ m is due to the radial temperature distribution. The appearance of a maximum followed by a minimum and then followed by a maximum for R_0 = ∞ m is due to the reasons given in Fig. (3). Due to the great width of the laser radiation more of the wings will be truncated leading to smaller temperature for $R_0=10^{-4}$ m than the linear case of $w_0=10^{-4}$ m part[I]. For $R_0=5X10^{-4}$ m the increase of the width of the laser radiation reduces the intensity more than the gained from the increased amplification leading to smaller temperature than the linear case of $w_0=10^{-4}$ m. For the other R_0 values the increase of the width, due to the behavior of $(\beta_L - \alpha_L)$, leads to a greater temperature than the linear case. That the temperature in this case is greater than the case of $w_{o}{=}10^{\text{-4}}\text{m}$ is due to the smaller width of the laser radiation after the minimum width compared with $w_0 = 10^{-4}$ m and the location of the minimum width is in this case closer to z=L.

Figure (8) represents the axial temperature distribution calculated at $t = \Delta t_p / 4$, r=0 and R_o as a parameter. For R_o=10⁻⁴ m the temperature at z=0 attains a greater value than its neighbors this value continue to decrease till the vicinity of the minimum width of the laser radiation where the temperature increases rapidly to reach its maximum value at z=0.06 m. This behavior is explained in Fig. (4). After reaching the temperature its maximum value it begins to decrease. This is because of the increased width leading in one hand to the reduction of the intensity of the laser radiation and on the other hand, due to the negative value of $(\beta_I - \alpha_I)$, to cut off its wings. For the other R_o values, the temperature at z=0 is smaller than at greater z values. This is due to the behavior of $(\beta_1 - \alpha_1)$ and the effect of self-focusing which leads the temperature for $R_0=5X10^{-4}$ m to have a maximum at z=0.07 m. For the other R_0 values the maximum is at z=L. This is due to the great radial amplification which overcompensates the reduction of the intensity resulting from the increase of the radius as well as accumulation of the heat energy at small times (linear behavior).



Fig. (7): The temporal temperature distribution induced by a laser beam having spatial intensity distribution of increasing width with increasing z – value (Gaussian beam) originating from a laser oscillator 0.1 m long, laying 0.1m a part from a laser amplifier. The Gaussian beam has a width of $1.77X10^{-4}m$ at the input of the laser amplifier. The calculation was carried out considering self-focusing at z = L, r = 0 and R_o as a parameter. Considering amplified power. $R_o = 10^{-4}m$ curve A $R_o = 5X10^{-4}m$ curve B $R_o = 10^{-3}m$ curve C $R_o = \infty m$ curve D

Figure (9) represents the radial temperature distribution calculated at $t = \Delta t_p / 4$, z=L and R_o as a parameter. The curves behave in relative distribution generally as those given in Fig. (5) except that the temperature in this case is greater. This is due to the greater cross-section of the laser beam allover the time except at times during which self-focusing occurs and at at which laser cross-sections are practically the same. Due to the smaller width of the laser radiation at z=L and the greater distance over which the width of the laser radiation in this case is smaller than the case of self-focused Gaussian distribution having w=10⁻⁴m and represented in Fig. (5), the temperature in this case is higher.



Fig. (8): The temperature distribution as a function of z induced by a laser beam having spatial intensity distribution of increasing width with increasing z – value (Gaussian beam) originating from a laser oscillator 0.1 m long, laying 0.1m a part from a laser amplifier. The Gaussian beam has a width of $1.77X10^{-4}$ m at the input of the laser amplifier. The calculation was carried out considering self-focusing at t = $\Delta t_p/4$, r = 0 and R_o as a parameter. Considering amplified power. $R_o = 10^{-4}$ m curve A $R_o = 5X10^{-4}$ m curve B $R_o = 10^{-3}$ m curve C $R_o = \infty$ m curve D



Fig. (9): The radial temperature distribution induced by a laser beam having spatial intensity distribution of increasing width with increasing z – value (Gaussian beam) originating from a laser oscillator 0.1 m long, laying 0.1m a part from a laser amplifier. The Gaussian beam has a width of 1.77×10^{-4} m at the input of the laser amplifier. The calculation was carried out considering self-focusing at t = $\Delta t_p/4$, z = L and R_o as a parameter. Considering amplified power. R_o= 10^{-4} m curve A R_o= 5×10^{-4} m curve BR_o= 10^{-3} m curve C R_o= ∞ m curve D

5. Conclusion:

The location at which the minimum width was observed was found to move towards greater z values as the width of the laser radiation was increased. The axial temperature was found to increase with increasing w_o value for $R_o > 5X10^{-4}m$.

6. Reference:

- 1. Haber, F.E. and Cohen, M.I. Solid-State Electtron[®] 11, (1968) 1176.
- **2.** Ready, J. F. Effects of high power laser radiation " Acadimic press New York (1971) .
- 3. Breinan, E. M., Kear, B. H. and Banas, C. M. Processing materials with *laser*. *Phys. Today* **29** (1967) 44.
- **4.** Charaschan, S. S., Laser Industry" Van Nostrand, New York (1972) chaps. 4 and 5.
- Porteus, J. D. and Decker, D. L., Metal mirror damage and precision diamond-turning". In laser induced damage in optical material (A. J. glass and A. H. Guenther, Eds) Academic press, New York (1980).
- 6. Porteus, J. D., Choyke, W. J. and Hollman, R. A., *Pulsed laser damage characteristic of vapor-deposited copper mirrors on silicon carbide substrate*". Appl. Opt. vol. **19**, 451 (1980).
- 7. Koechner W. *Solid-state laser engineering*, 4th ed. Berlin: Springer, p. 381 (1992).
- **8.** Comasky B, Moran BD, Albrecht GF and Beach RJ. Characterization of heat loading of Nd: doped YAG, YOS, YLF, and GGG excited at diode pumping wavelength. IEEE J Quantum Electron; **31**, 1261 (1995).
- **9.** Sliney JG, Leung KM, Birnbaum M and Tucker AW. Lifetimes of the 4F3=2 state in Nd:YVO4. *J. Appl Phys* **50**(5):3778–9 (1979).
- P:stner C, Weber R, Weber HP, Merrazzi S and Gruber R. Thermal beam distortion ins in end pumped Nd:YAG, Nd:GSGG and Nd:YLF rods. *IEEE J Quantum Electron*; 30, 1605 (1994).
- Jabczynski JK, Kopczynski K and Szczesniak A. Thermal lensing and thermal aberration investigations in diode-pumped lasers. Opt Eng; 35(12):3572 (1996).
- 12. V. Spagnolo, M.Troccoli, G. Scamarcio, C. Becker, G. Glastre and C. Sirtori " *Facet temperature mapping of GaAs/AlGaAs quantum cascade lasers by photoluminescence microprobe* " Optical Materils 17, 219 (2001).
- **13.** G. Romo, T. Smy, D. Walkey and B. Reid "*Modeling facet heating in ridge lasers*" Microelectronics Reliability 43, 99 (2003).

14.	Kosterin, Andrey; Erwin, J. Kevin and Fallahi, Mahmoud;
	Mansuripur, Masud " Heat and temperature distribution in a cladding-
	pumped, Er: Yb co-doped phosphate fiber " Review of Scientific
	Instruments, Volume 75, Issue 12, pp. 5166-5172 (2004).

- **15.** Ready . G.F. "*Effects due to absorption of laser radiation*" J.Appl. Phys **36**, 462 (1965).
- 16. Hassan. A. F. etal "Heating effects induced by a pulsed laser in a semiinfinite target in view of the theory of linear system" Optics & Laser Technology Vol. 28 No. 5, 337 (1996).
- 17. Peter W. Milonni and Joseph H. Eberly "Lasers" Rochester, New York, John Wily & Sons (1988).
- **18.** M. M. El-Nicklawy, A. F. Hassan, El. M. A. Nasr, A.A. Hemida and S. M. El-Genedy "Two dimensional temperature distribution resulting from propagation of a light beam through an amplifying medium Part 1: linear case" To Be Published