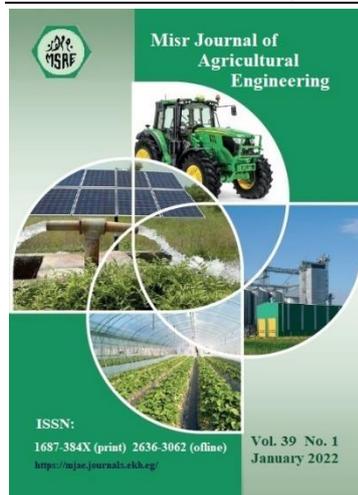


ENHANCEMENT OF SOLAR STILL EFFICIENCY BY USING CELLULOSE COOLING PAD AND WATER SPRINKLER

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Solar still; Sprinkler;
Cooling pad.

ABSTRACT

Study aims to overcome low productivity of solar still by using cellulose cooling pad and water sprinklers to increase water evaporation. Three identical solar stills were used under climatic conditions of Egypt at Ismailia city. Solar stills were designed, installed, and tested at the Agricultural Engineering Department, Faculty of Agriculture, Suez Canal University, Ismailia Governorate, Egypt. The solar still basin made of galvanized iron sheet, with a net upper surface area of 1.04 m². A clear glass cover of 3 mm thick was placed and inclined by a tilt angle of 31°. It was painted with matt black paint to absorb the maximum possible amount of solar radiation incident on it. The first conventional solar still was used as a control unit (S1). The second still was functioned with the cooling cellulose pad (S2). The third still was operated with the water sprinklers to spray saline water (S3). For the duration of the experimental tests, the hourly average volumetric thermal efficiency was 31.5, 40.1 and 44.2 % for the S1, S2 and S3, respectively.

1. INTRODUCTION

Fuels are the world main energy resource and considered the center of energy demands. However, reserves of fossil fuels are limited and their large-scale use is associated with environmental deterioration. These facts have encouraged growth in the use of renewable energy resources (Taha and Helal 2020). To solve dependency on fossil fuels researchers and governments are working tirelessly on renewable energy which should be commercially viable, pollutant free and must be abundant in nature (Chukwujindu, 2017). The energy from the sun intercepted by the earth is many thousands of times larger than the present consumption rate on the earth of all commercial sources (Nandurkar and Shelke, 2012). One of the simplest and most direct applications of this energy is the conversion of solar radiation into heat (Kishk and Abu-Zeid 2019). The solar distillation is one of the most important methods for producing fresh water from brackish and sea water using the free and friendly energy supply (solar energy). Supplying fresh and healthy water is still one of the major problems in different parts of the world, especially in arid remote areas. Solar stills can solve a part of the problem in those areas where solar energy is available (El-Sheikh and Kishk, 2016). Supplying fresh and healthy water is still one of the major problems in different parts of the world, especially in arid remote areas. Solar still is one of the best solutions to

solve water problem in remote arid areas. This device is not popular because of its lower productivity. One of the methods to increase the productivity is by increase the water evaporation area. The solar distillation is one of the most important methods for producing fresh water from brackish and sea water using the free and friendly energy supply (solar energy). These units can be placed at each house for producing at least drinking water (**Arjunan et al., 2009**). Solar desalination is a process of separating pure water from saline water using solar energy (**Sakthivel et al., 2010**). This inexpensive device can easily be built using local materials (**Kantesh, 2012**). There is a strong need to improve the solar still performance and increase the production of water distillation (**Sundaram et al., 2016**). Single slope solar stills are one of the solar devices used for freshwater production. They are considered as one of the cheapest solutions for purifying saline water and suitable for the Middle East and Africa due to their easily constructive approach and maintenance (**Goosen et al., 2000**). **Kabeel et al. (2010)** used different methods and modifications to improve the productivity of solar stills. The results showed that the best average and maximum daily productivity are obtained from solar stills of single slope shape. **Bassam et al. (2003)** proposed a modification to enhance the distillate production by placing sponge cubes over the water surface. The sponge cubes increased the surface area over which evaporation of water occurs hence caused the increase of yield by 18%. The cover with inclination equal to latitude angle will receive the sun rays close to normal throughout the year. For places with latitude higher than 20°N, single slope still is preferable (**Fath et al., 2003**). Heat transfer within the solar still depends mainly on the evaporative surface area and the temperature difference between the evaporative surface temperature and the condensing surface temperature (**Rai et al., 2013**). **Singh and Tiwari (2004)** found that the annual yield of the solar still was maximized when the condensing glass cover inclination is equal to the latitude of the place. **Abd Elkader (1998)** found that the optimum inclined angle for solar still was 30-35° for Port Said/Egypt (latitude angle of 31.2°N). **Murugavel et al. (2008)** found that the solar still with glass cover plate with 3 mm thick gives 16.5 % more production than that covered with 6 mm thick glass cover. The basin water depth is also having a significant effect on productivity of the basin. Experiments with deep basin reveal that the productivity of the still decreases with an increase in depth of water during daylight (**Rajesh and Tiwari, 2005**). **Phadatare and Verma (2007)** studied Influence of water depth on internal heat and mass transfer in a plastic solar still. Investigations show that, the water depth is inversely proportional to the productivity of still. **El-Zahaby et al. (2011)** studied the still performance using a spray feeding system. They found the sprayed system improving the performance along the whole daytime and, particularly, on the morning hours. Several works were carried out by researchers, to improve the production capacity of the still, by adopting different techniques. The basin water depth is having significant effect on productivity of the solar still. Investigations show that, the water depth is inversely proportional to the productivity of still (**Phadatare and Verma, 2007**). If the water surface in the basin is exposed to larger area, the evaporation rate is high. The water surface area can be increased by employing suitable wick and porous materials in the basin. The performance of a solar still with different size of sponge cubes placed on the basin was studied experimentally by (**Abu-Hijleh and Rababa'h, 2003**). The increase in distillate production of the still was from 18% to 27% compared to a

conventional still. The study is aimed to overcome the low efficiency of solar still by using cooling cellulose pad and water sprinkler to increase the saline water evaporation, under climatic conditions of Egyt at Ismailia city.

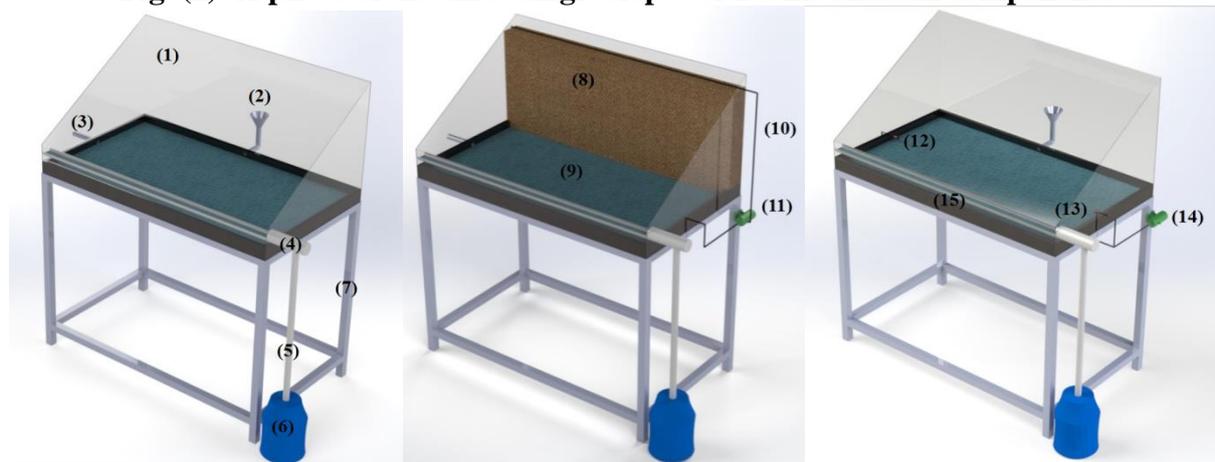
2. MATERIALS AND METHODS

Experimental setup

Three simple basin-type solar stills each having similar basin area were constructed and tested at Department of Agricultural Engineering, Faculty of Agriculture, Suez Canal University, Ismailia Governorate, Egypt (latitude angle of 30.62°N, Longitude angle of 32.27°E, and mean altitude above the sea level of 5 m). The schematic diagram and the pictorial view of the solar still units and components are shown in **Figs (1 and 2)**, respectively. The geometric characteristics of each still are as follows: width, 0.8 m, length, 1.3 m, basin depth, 0.1 m, basin surface area, 1.04 m². The still basin shape is rectangular and made of galvanized iron sheet. It is painted by matt-type black to maximize the absorbed solar radiation. A clear glass cover of 3 mm thick was placed and inclined by a tilt angle of 31° to transmit the maximum possible of solar radiation flux incident on it (**Singh and Tiwari, 2004**).



Fig. (1): A photo of the three single slope solar stills and still components



- | | | | |
|-----------------------------|----------------------|------------------------|-----------------------|
| 1- Glass cover | 2- Feed saline water | 3- Salt water drainage | 4- Collecting channel |
| 5- Distillate outlet vessel | 6- Distillate water | 7- Frame | 8-Cellulose pad |
| 9-Saline water | 10- Inlet pipe | 11- Water pump | 12- Sprinkler |
| 13- Sprinkler | 14- Water pump | 15- Wooden box | |

Fig. (2): Schematic diagram of experimental setup of solar stills

The slope was adjusted to 31° , which is considered adequate for geographical location of Ismailia city. With this inclined angle (31°), the condensates will run down underneath the glass cover into the trough rather than dropping from the cover into the basin. Glass cover has been sealed with silicone rubber which plays an important role to promote efficient operation of condensation as it can accommodate the expansion and contraction between dissimilar materials. To minimize heat loss from the base and the sides of the still basins, each galvanized basin was fitted inside a wooden frame. The gaps between each wooden and galvanized basin were packed with 0.05 m thick of rock wool (thermal conductivity = $0.0346 \text{ Wm}^{-1}\text{K}^{-1}$) for the outside walls and bottom. To collect the distilled water from the solar still, a trough made from PVC was placed along the bottom side of the glass cover with an inclination of 5° towards the collecting head to speed up the condensate velocity and to avoid the tendency of re-evaporation. The system has capability to collect distillates from all sides of the solar stills. The distilled water is continuously collected in a plastic vessel located outside the still and measured using a graduated cylinder. A steel pipe is used to supply the saline water fixed at the side wall of the still for feeding saline water. The cooling cellulose pad system consists of cellulose pad and water pump connected with still basin by fixable plastic tube (6 mm diameter). Cellulose pad plate has a gross dimension of 40 cm high, 120 cm wide and 10 cm thick with net surface area of 0.48 m^2 . Cellulose pad plate placed vertically in the opposite inclined wall (Northern direction) in the solar still.

Water can be recycled to the cellulose pad by a DC water pump (30 W, 24 V, and 2 litres per minute discharge). The pump related to plastic pipe installed on the upper part of pad to recirculate water from the basin to the pad again. Twenty holes were drilled about 6 cm apart along the top side of plastic pipe, and the end of this pipe was capped. The spray system consists of two sprinklers installed at the sides of solar still and connected with the still basin by a DC water pump (30 W, 24 V) and fixable plastic tube (6 mm diameter) to recirculate water from basin to the sprinklers again. The saline water is continually sprayed at constant flow rate 65 ml/min for each sprinkler. Photovoltaic module of a nominal power of a 75 W and circuit voltage 24 V was used within the experimental task of this study. The module was made by Siemens Solar Company, American made. The solar stills and solar module were faced the south direction and inclined by a tilt angle of 31° to transmit the maximum possible of solar radiation flux incident on it.

Measurements and data acquisition

The investigation was carried out on sunny days throughout July month of summer 2020 under Ismailia city climatic conditions. The experiments were conducted from sunrise to sunset and all the three stills were operated simultaneously. The experimental procedure commenced by cleaning dust from the external glass covers and the collected water was measured each one hour during daylight. Meteorological station (Vantage Pro 2, Davis, USA) located above the roof of the Agricultural Engineering Department was used to measure different macroclimate variables such as solar radiation flux incident on a horizontal surface (pyranometer), dry-bulb, wet-bulb, and dew-point air temperatures as shown in **Fig (3)**. Twelve thermocouples with a range of 0 to 100°C with an accuracy of $\pm 0.1^\circ\text{C}$ were functioned to measure the temperatures of various points of each solar still system (basin water temperature (T_w) vapour temperature (T_v) inside glass temperature and ambient air

temperature (T_a). These sensors were connected to a data-logger system (a 12-channels data logger device, Digi-sense scanning thermometer type) to display, and record the data during the experimental period.



Fig. (3): Meteorological station and data logger system

Methods

Experiments were carried out under prevailing weather conditions of Ismailia region during July month of 2020. By keeping the depth of water in the basin at 2 cm (21 liter). During operating the solar stills, solar radiation was transmitted through the glass cover and absorbed by both the brackish water and the black metallic basin. Part of the absorbed energy by the basin is transferred by convection to the saline water. Condensate water was flowed by gravity into the collection trough at the lower edges of the tilted glass cover. Suez Canal water (34,500 ppm) was used as feed. The yield from the still was collected and measured everyone hour during the daytime. The first conventional solar still was used as a control unit (S1). The second still was functioned with the cooling cellulose pad (S2). The third still was operated with the water sprinkler to spray saline water (S3). The concentration of hydrogen ion (pH), electrical conductivity (EC, $\mu\text{s}/\text{cm}$), and total dissolved solids (TDS, ppm) of the brackish water, respectively, were 7.8, 48.5 $\mu\text{s}/\text{cm}$ and 31040 ppm.

Thermal efficiency of the solar still

The thermal efficiency of the solar still from the experimental measurements (volumetric thermal efficiency) which represents the productivity of fresh water was mainly computed using the following formula **Kantesh (2012)**:

$$\eta = \frac{m \cdot L}{3.6 (A \cdot I)}$$

where, m is the rate at which distillate of fresh water is produced from the still in kg h^{-1} , L is the latent heat of vaporization in kJ kg^{-1} at an average basin water temperature (T_w), A is the surface area of basin in m^2 , and I, is the solar radiation flux incident on the basin in W m^{-2} .

The average latent heat (L) was determined by **Kabeel and Abdelgaied, (2016)** as follows:

$$L = 10^{-3} (2501.9 - 2.40706 T_w + 1.192217 \times 10^{-3} T_w^2 - 1.5863 \times 10^{-5} T_w^3)$$

3. RESULTS AND DISCUSSION

For the duration of the experimental work, the three solar stills were operated satisfactorily without malfunction. The measurements of solar radiation intensity, various temperatures, and the production of distilled water were taken each hour. By keeping the depth of water in the basin at 2 cm (21 liter). Average ambient air temperature and solar radiation intensity during July month of 2020 are shown in **Fig. (4)**. The intensity of solar radiation was gradually

increased from sunrise (144 Wm^{-2}) till reached the maximum value (739 Wm^{-2}) at 13.00 h, then it gradually decreased until approached the minimum value (142 Wm^{-2}) prior to sunset. The average intensities of solar radiation were 475.7 Wm^{-2} . While the ambient air temperature increased gradually from 27.4°C at 7.00 h until reached the maximum value (35.2°C) at 13.00 h, then it was decreased till reached 27.5°C at 19.00 h. During the experimental period, the hourly average ambient air temperature was 32.1°C .

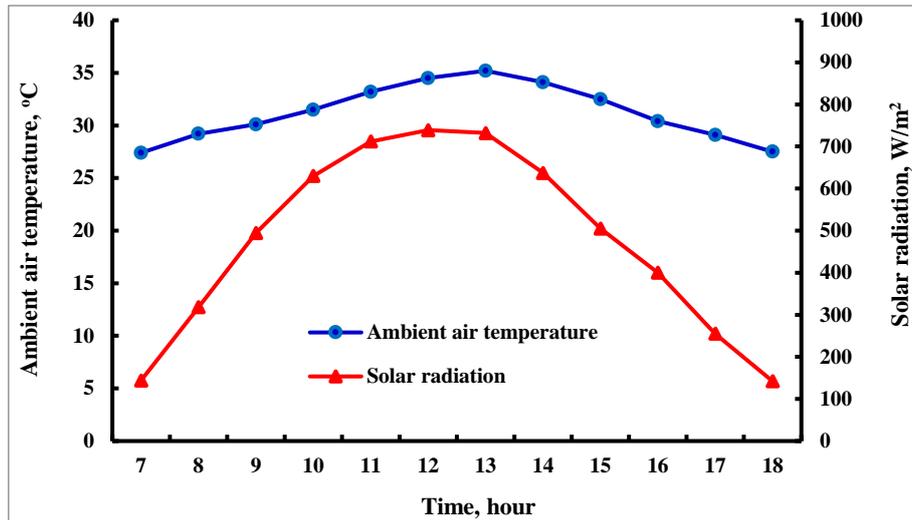
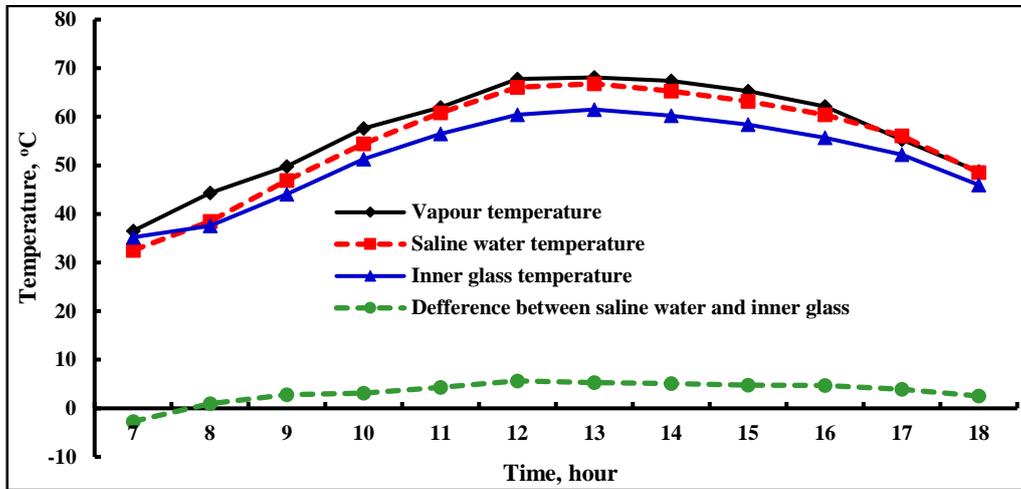


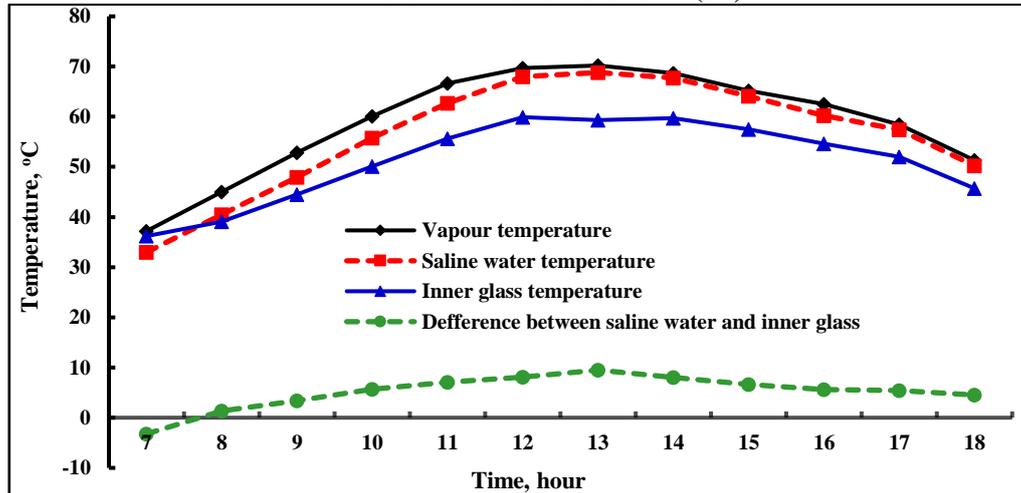
Fig. (4): Hourly average ambient air temperature and solar radiation during July month of 2020

The variations in temperatures at different locations of three different solar stills are presented in **Fig. (5)**. As shown from the illustration, the temperatures have the same trend, as they increased in the morning hours and attain maximum values at around 13:00 h and decreased in the evening hours. This is obviously since the solar incident radiation increased in the morning but decreased in the afternoon. The vapour temperature had the largest temperature because the particles of vapour have enough heat energy (comprises sensible and latent heat) to evaporate. The highest vapour temperature was obtained between 13:00 pm and 14:00 h for all solar stills. It is noticed also that the average vapour temperature was found to be 57.1 , 59.0 and 59.4°C for the S1, S2 and S3, respectively. From **Fig. (5)** it can clearly be seen that saline water temperatures increased for all tested solar stills reached the maximum values of 66.8 , 68.8 and 69.3°C for the S1, S2 and S3, respectively in afternoon (13.00 h) because to the absorbed solar radiation exceed the losses to the surrounding. After 13.00 h, saline water temperature decreased because the heat energy losses from the solar stills which became larger than the absorbed solar radiation. Average saline water temperatures for solar stills around the daytime with one hour interval were found to be 55.0 , 56.3 and 57.0°C for the S1, S2 and S3, respectively. The water temperature depends strongly upon the other different parameters such as the intensity of solar radiation, absorptivity of the water and black basin surface, and temperature difference between the water vapour and inside surface of the solar still. Also, **Fig. (5)** shows the effect of cellulose cooling water and spray water inside still on the inner glass cover temperature. It can be also noticed from **Fig. (5)** that the glass cover temperature was usually lower than that of the water temperature except in the early morning when the difference between them was very small. As the glass cover temperature is much lower than the water vapour temperature, it caused condensation of vapour on the internal

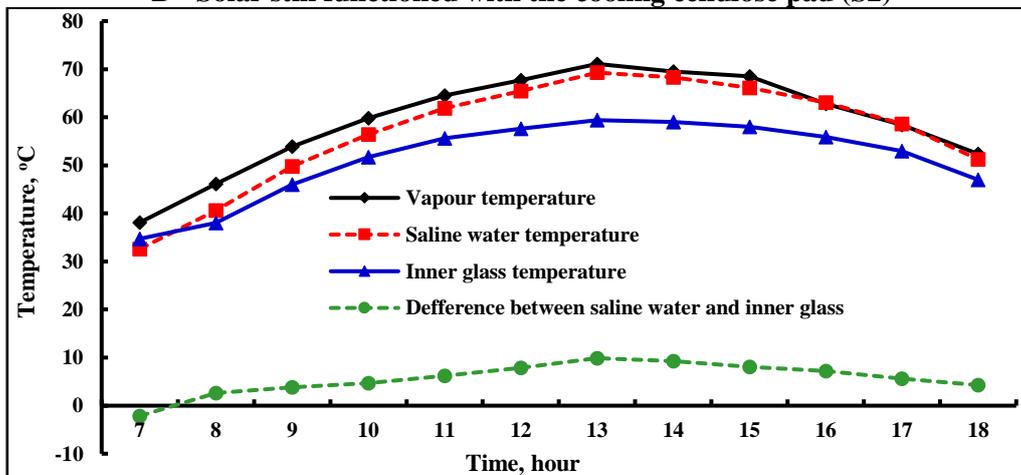
surface of the glass. In the early morning hours (7.00 - 8.00 h), the glass temperature was close to the water and vapour temperatures resulting in small productivity due to the small heat energy absorbed by the water at these times.



A - The conventional solar still (S1)



B - Solar still functioned with the cooling cellulose pad (S2)



C - Solar still operated with the water sprinkler (S3)

Fig. (5): Hourly variation in temperature of solar stills

The hourly average inner glass temperatures for solar stills were found to be 51.6, 51.2 and 51.4°C for the S1, S2 and S3, respectively. The difference in temperature between saline water and inner glass throughout the day for the solar stills is plotted in **Fig. (5)**. During early morning glass cover encountered the solar radiation first and its temperature rose very fast with time as compared with the rising in water temperature, and as a result the difference becomes negative. These differences remain negative till water temperature exceeded glass temperature. The maximum positive difference was found to be 5.7, 9.5 and 9.9°C which achieved at 14.00 h S1, S2 and S3, respectively, after that the difference decreases till the sunset. The economical productivity rate of fresh water reflects how much the solar stills were adapted to the increase evaporation area. The yields ml/m² hr for the different solar still trials are shown in **Fig. (6)**. The productivity of fresh water for the three solar stills gradually increased from early morning until reached the maximum values (495, 565 580 ml/m².hr, respectively) afternoon then they decreased till approached the minimum values (100, 135, and 158 ml/m².hr) just prior to sunset. The cooling cellulose pad and spray water can be considered as one of the parameters that has a direct effect on the productivity of fresh water.

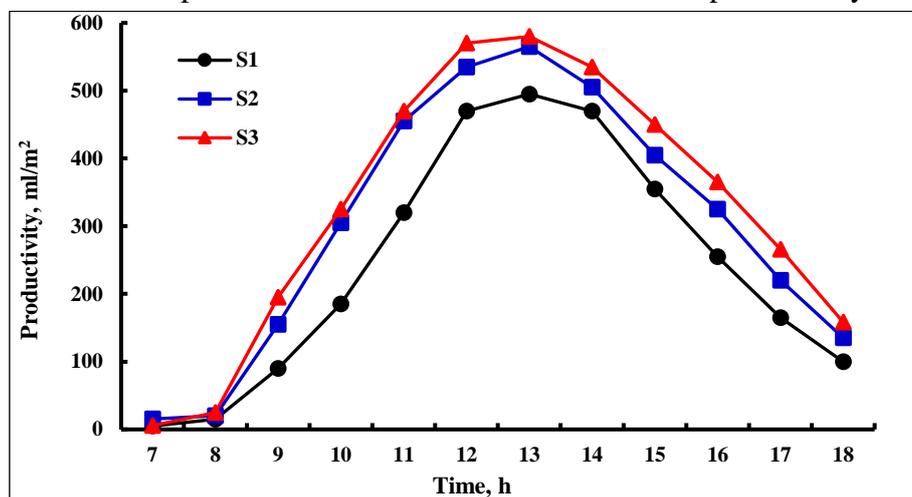


Fig. (6): Hourly average volumetric production rate as a function of solar time.

Daily average production of fresh water under the three different solar stills (S1, S2 and S3 stills), respectively, were 244, 303 and 329 ml/hr. Results showed that, the solar intensity is directly proportional to the yield of fresh water from the solar still due to the increase in heat energy gained by the saline water at which vaporization inside the stills increased (**Sathyamurthy et al., 2014**). In the other hand, the accumulated freshwater yield for the solar stills depicts in **Fig. (7)**. The total daily productivity of fresh water from the three solar stills approximately reached to 2925, 3640, and 3944 ml/m² day, for the S1, S2 and S3, respectively. This means that, the cooling cellulose pad and spray water increased the average production by 24.5 and 34.9 % as compared with the control solar stills, respectively. The experimental results showed that, the daily average productivity of fresh water for the two solar stills with cooling cellulose pad and spray were higher than that of the conventional solar still. The highest productivity rate was achieved from the solar still with spray were due to the higher evaporative surface area. As a result, using cooling cellulose pad and spray in solar still was found to be the best option to increase the solar still productivity during the daylight-time.

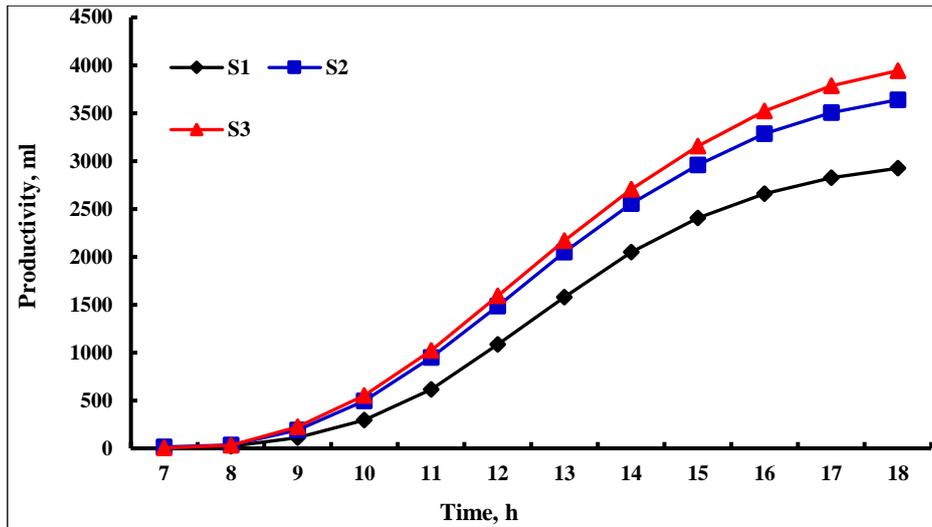


Fig. (7): Effect of PCM on the accumulated productivity of solar stills

The volumetric thermal efficiency of the solar still is considered the most important factor for evaluation because it can reveal the best solar still operation. The hourly average volumetric thermal efficiencies for each solar still type within a representative day under the average weather conditions are plotted in Fig. (8). In the same trend, the volumetric thermal efficiencies for the three solar still increased with the time until reaching the maximum value afternoon. For the duration of the experimental tests, the average solar still volumetric efficiency was found to be 31.5, 40.1 and 44.2 % for the S1, S2 and S3, respectively. The results show that the volumetric thermal efficiency and productivity of solar still are directly proportional.

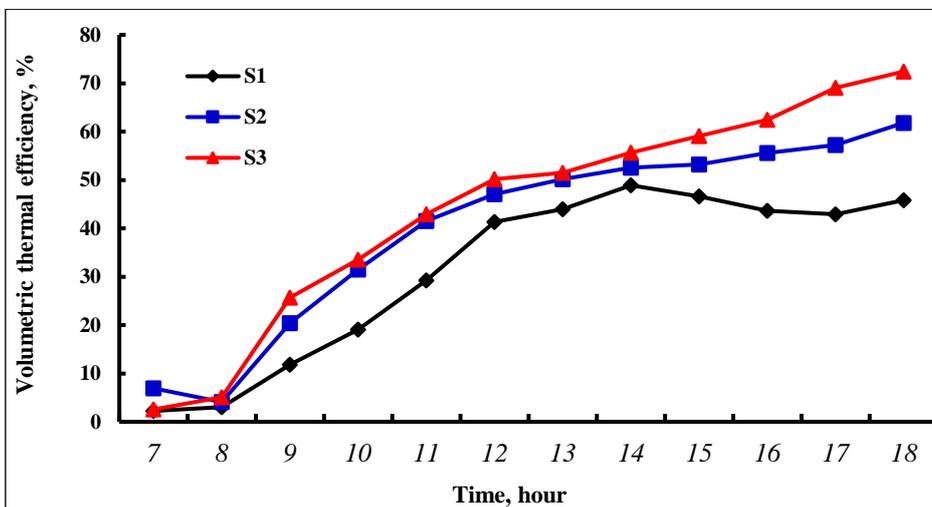


Fig. (8): Hourly average volumetric thermal efficiency versus time for the solar stills

Distilled Water Quality

The pH, EC and TDS values of the sea water and the water distilled which obtained from the experimental work are summarized and listed in Table (1). These values were found to be much lower (7.46, 0.21 $\mu\text{s}/\text{cm}$ and 134.4 ppm, respectively) than those of the sea water (7.8, 48.5 $\mu\text{s}/\text{cm}$ and 31040 ppm, respectively). The quality of potable water distilled from solar still is suitable for drinking particularly in remote areas.

Table (1): Quality parameters (pH, EC, and TDS) of the solar distilled water and sea water during the experimental tests

Parameter	Sea water	Distilled water
pH	7.8	7.46
Electrical conductivity (EC), $\mu\text{s}/\text{cm}$	48.5	0.21
Total Dissolved Solids (TDS), ppm	31040	134.4

4. CONCLUSION

In this present research work, several conclusions can be obtained and drawn as follows:

- 1- Daily average production of fresh water under the three different solar stills (S1, S2 and S3 stills), respectively, were 244, 303 and 329 ml/hr. This means that, the cooling cellulose pad and spray water increased the average production by 24.5 and 34.9 % as compared with the control solar stills, respectively.
- 2- The total daily productivity of fresh water from the three solar stills approximately reached to 2925, 3640, and 3944 ml/m² day, for the S1, S2 and S3, respectively.
- 3- The pH (7.46), EC (0.21 $\mu\text{s}/\text{cm}$), and TDS (134.4 ppm) values were lower than those of the brackish water (7.8, 48.5 $\mu\text{s}/\text{cm}$ and 31040 ppm, respectively).
- 4- Using cooling pad and spray in solar still was found to be the best option to increase the solar still productivity during the daylight-time.
- 5- The hourly average solar still thermal efficiency was 31.5, 40.1 and 44.2 % for the S1, S2 and S3, respectively

Finally, to overcome low productivity of solar still we can use cellulose cooling pad and water sprinklers to increase solar still efficiency.

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تحسين كفاءة المقطرات الشمسية باستخدام وسائد التبريد ورشاشات المياه

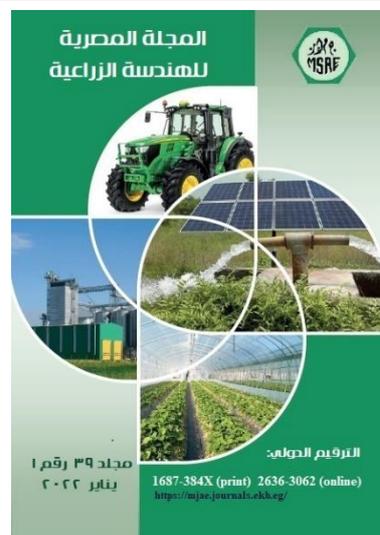
سامح سعيد كشك^١^١ أستاذ مساعد - قسم الهندسة الزراعية - كلية الزراعة - جامعة قناة السويس

الملخص العربي

تتلخص المشكلة البحثية في نقص إنتاجية المقطرات الشمسية وبالتالي ضعف كفاءتها الحرارية - ويهدف البحث إلي زيادة إنتاجية وكفاءة وحدات التقطير الشمسي عن طريق زيادة تبخير باستخدام وسائد التبريد ورشاشات المياه. أجري هذا البحث بقسم الهندسة الزراعية - كلية الزراعة - جامعة قناة السويس. حيث تم إنشاء ثلاث وحدات متماثلة من وحدات التقطير الشمسي ذات الميل من الجانب الواحد. تتكون الوحدة من حوض مصنوع من الصاج المجلفن بسبك ١ مم وبمساحة سطحية ١,٠٤ م^٢ وعمق ٠,١ م تم طلاؤه باللون الأسود لزيادة امتصاصية الأشعة الشمسية والحوض مثبت داخل صندوق مصنوع من الخشب بسبك ٠,٠٢ م، تم عزل الحوض المعدني من الجوانب ومن أسفل بطبقة من الصوف الزجاجي سمكها ٠,٠٥ م. أما سطح التكتيف الرئيسي فهو عبارة عن غطاء من الزجاج الشفاف بسبك ٣ مم يميل بزاوية مقدارها ٣١° على الأفقي موجه ناحية الجنوب. القطرات المتكاثفة بالداخل يتم تجميعها من خلال قناة التجميع الموجودة أسفل الغطاء الزجاجي. تم تغذية الوحدات الثلاث بمياه مالحة من قناة السويس. تم إنشاء نظامين لزيادة تبخير الماء المالح. النظام الأول مكون من وسادة مصنوعة من السيلولوز بسبك ٠,١ م وطول ١,٢ م وعرض ٠,٤ م بمساحة سطحية كلية ٠,٤٨ م^٢ متصلة بمضخة (قدرة ٣٠ وات) تقوم بضخ الماء المالح من الحوض في أنبوبة مثقبة أعلى سطح الوسادة بمعدل تدفق ٢ لتر/ دقيقة لتوزيع الماء المالح بانتظام أعلى الوسادة. النظام الثاني مكون من زوج من رشاشات الماء مثبتة على جانبي الحوض تقوم بتحويل المالح الى قطرات صغيرة مما يسهل من عملية التبخير تصرف الرشاش الواحد ٦٥ مل/ دقيقة وقد صممت التجربة بحيث تكون الوحدة الأولى وحدة تقليدية ككنترول، الوحدة الثانية مضاف إليها وسادة التبريد، الوحدة الثالثة تحتوي على رشاشات المياه.

وقد أوضحت النتائج ما يلي:

- ١- متوسط الإنتاجية خلال اليوم ٢٤٤، ٣٠٣ و ٣٢٩ مل/ م^٢ ساعة للوحدة الأولى والثانية والثالثة على الترتيب. وبالتالي نظام الوسادة ورشاشات الماء أدى لزيادة الإنتاجية بنسبة ٢٤,٥ و ٣٤,٩ % مقارنة بالوحدة الكنترول
- ٢- الإنتاجية الكلية للوحدات الثلاث خلال اليوم ٢٩٢٥ و ٣٦٤٠ و ٣٩٤٤ مل / م^٢ يوم للوحدة الأولى والثانية والثالثة على الترتيب
- ٣- استخدام وسائد التبريد ورشاشات الماء كوسيلة تبخير الماء أدى الى زيادة كلاً من الإنتاجية وكفاءة التشغيل لمقطرات الماء الشمسية. في النهاية يمكن التوصية باستخدام وسائد التبريد ورشاشات الماء داخل وحدات التحلية كوسيلة لزيادة تبخير الماء وبالتالي زيادة كفاءة وحدات التقطير الشمسي.



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الكلمات المفتاحية:

المقطرات الشمسية؛ رشاشات مياه؛ وسائد تبريد