

PERFORMANCE EVALUATION OF PORTABLE MACHINE FOR TURF GRASS SHEAR

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ABSTRACT

The main objective of this study is to evaluation and develop the cutter blade of the portable machine for turf grass shear to increase its shearing efficiency, used in garden and club selfsame small areas and estimate the operation cost. The performance of portable machine for turf grass shear in terms of field efficiency, cutting efficiency, energy requirements and shearing cost were investigated dependent on change in kinematics parameter (ratio of knife peripheral velocity to machine forward speed), knife types (fixed imported cutting blades and free modified free cutting blades) with three and four cutter blade during the shearing operation .The operating shear a kinematic parameter of 290 which corresponded to forward speed of 0.25 m/s, knife velocity of 72 m/s was the optimum. The best adjusting of the knife of the machine at cutting height of 4 cm with moisture content 40 % was used free modified knife with three cutter blade.

INTRODUCTION

Turf grass in golf courses, clubs, public garden and stadiums play a vital role in population life. Turf grass refines the atmosphere from the bad particles which cause pollution in the air. The green bed refines the atmosphere from the bad particles of pollution in the air. Green bed is used widely as a playground for most games in different clubs. This process is still operated depending on primitive methods using manual tools or imported machines of highly cost. So, turf grass cutting by means of up to date technology taking into consideration **Morad 1995**) .Machine performance, field efficiency, fuel requirements and operating cost is an important. Many researches were carried out on the rotary mechanisms of cutting machines and the design variables which affect the cutting efficiency. **Prasad and Gupta (1973)** found that the cross section area and moisture content of the cut material had significant influence over shearing energy and maximum shearing force.

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Mored (1981) found that the required force for cutting any material may be divided into two parts. The first part is the inertia force required to move the cutting mechanism, and the second is the shearing force required to shear the material. Inertia force is affected by the square of knife velocity resulting in a sharp increase of cutting energy. The force was found to be affected by knife velocity, machine forward speed, and material moisture content. **Awady et al. (1988)** reported that rotary disk with cutter blades gave better operation efficiencies (0.45-0.91). Appropriate tip speeds are determined according to forward speed, blade protrusion and other relevant factors. **Habib (2002)** Found that the cuttings force of the plant materials is the main parametric force affecting knife velocity. Whereas, the tension and bending forces that resulted in the plant stalk are of little effect on the cutting knife velocity. **El-Sahar (1988)** Indicated that the cuttings force is greatly affected by the diameter of the plant stem. For three types of plant stem of cotton, wheat and lawn, 625 N force was needed to cut of 9 mm cotton stalk diameter at 6.5 %, for 2.5 mm diameter lawn stems in bundles of four stems. Decreasing cutting forces at higher moisture contents were due to visibility of the stalk tissues of plant stems. **Imbabi (1992)** found that the energy requirements for cutting the sesame plants ranged from 4.32 – 27.03 Joule / stem according to the moisture content of stems, while the cutting force ranged from 432.14 – 1351.31 N/stem according to the moisture content of stems. **Kepner et al., (1982)** mentioned that peripheral speeds generally ranged from 51 to 76 m / s, but they were somewhat lower than for rotary cutters, they usually range from 46 to 56 m/s or less.

The objectives of the present research is:

1. Performance evaluation of portable machine used in turf grass shear to improve its performance and minimize the operation cost.
2. Selecting the optimum conditions (kinematic parameter) and the optimum cutting blade for operating the machine.

MATERIALS AND METHODS

In this study, the portable machine turf grass shear of CG520, Chine made (shoulder brush type) was used for with imported and modified blades under study. The blade modification process was manufacture at

some private workshop in Kafrelsheikh City, Egypt. The experiments were carried out in Kafrelsheikh City small garden during the year of 2017. .

A – Materials:

1 - Turf grass variety.

Experiments were carried out on Turf grass variety Paspalum this grass spread it"s cultivation in Egypt. The moisture content of Turf grass at the time of experiment was 40 % w.b.

2 - portable machine

- The portable machine installation used in this study as shown fig (1).

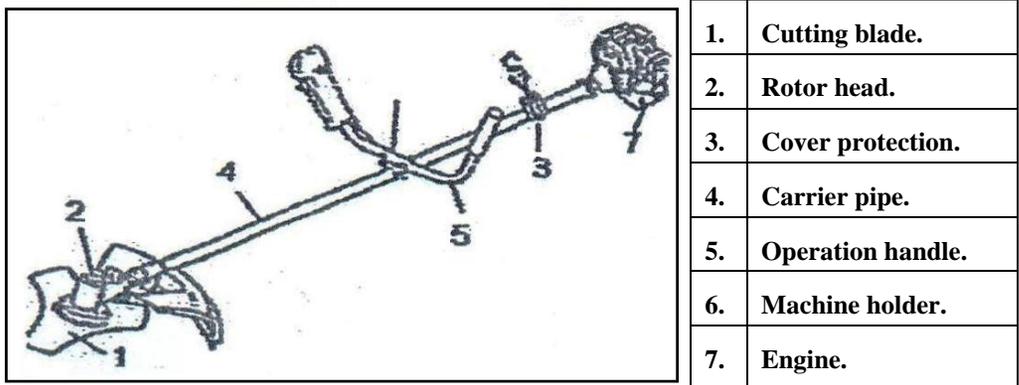


Fig (1): General view and main components of portable

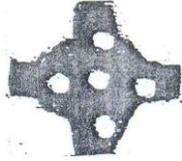
- Cutting blades

In this study, four shapes of cutting blades were used with portable machine turf grass shear. Two of them were imported blades, namely: 3 teeth and 4 teeth fixed blades. While, the other two blades were modified blades, namely: 3 teeth and 4 teeth free blades constructed on disc of diameter 185 mm. The main specification and components of these are summarized in Table (1).

– Rotor head and cover protection

The end of portable machine is the rotor head which was equipped with special setting for fixing cutter blade. The cover protection was fixed on the carrier pipe behind the cutting blade on the rotor head .

Table (1): The main specifications and components of cutting blades.

	imported blades		modified blades	
Shapes of cutting blades				
blade length, mm	70	35	70	35
blade width, mm	48	48	40	40
Working width, mm	255	255	255	255
No of teeth / blade	3 blade fixed / disc	4 blade fixed / disc	3 blade free / disc	4 blade free / disc

– Carrier pipe and connecting rod

The carrier was made from aluminum pipe with the length of 150cm and diameter 3cm . One of its ends was fixed with engine power output shaft through a centrifugal clutch and the other end fixed with rotor head. However, the connecting rod was passed through the carrier pipe and used to transmit the power between engine and rotor head which rotates the cutting blade.

– Operation handles and machine holder.

The operation handles were fixed on the carrier pipe to adjust the position of portable machine for turf grass shearing. Also, the operation components of stop switch, throttle lever and starting throttle lever latch were fixed on the right hand. However, the machine holder was used to carry the machine on the worker"s shoulder during cutting operation.

– **Engine.**

A small gasoline engine 1.4 kW, two strokes, and air cooled with overall sizes (Length x Width x Height)cm 181 x 33.5 x 32 was used as the power source for operating portable machine cutter.

B - Methods

The shearing experiments carried out to optimize some operating parameters affecting the performance of shearing machine these parameters are:

- Three Kinematic parameter of 180, 240 and 290 %.
- Two Knife types (imported and modified).
- Two Blade number (four and three).

1 - Kinematic parameter .

The Kinematic parameter was defined as the ratio of knife peripheral velocity to machine forward speed

$$\lambda = \frac{\omega r}{v}$$

Where:

λ : Kinematic parameter.

ω : Angular velocity of the knife, rpm

r : Rotor radius, m

v : Machine forward speed, m/s

The proper adjustment of the kinematic parameter during turf grass shearing is great importance to decrease turf grass cutting losses and consequently increase cutting efficiency.

There were three ways in which the kinematic parameter can be varied: change the knife velocity, and machine forward speed 0.25 m/s.

All experiments were run under a constant forward speed 0.25 m/s, and different knife velocity of 44, 62 and 72 m/s, which corresponded to different kinematic parameter of 180, 240 and 290 respectively as shown in table (2):.

The performance of the turf grass shearing machine was evaluated a change in kinematic parameter, knife types of imported and modified and blades number.

Table (2) Kinematic parameter used in portable.

Knife types	Blade number	Knife velocity m/s	Kinematic parameter %
imported	3	44	180
		62	240
		72	290
	4	44	180
		62	240
		72	290
modified	3	44	180
		62	240
		72	290
	4	44	180
		62	240
		72	290

C – Measurements:

Evaluation of the turf grass shearing machine performance was carried out by taking into consideration the following indicators.

1 - Field efficiency for the portable:

The field efficiency was calculated by using the following equation;

$$E_f = \frac{C_{ef}}{C_{th}} \times 100 \text{-----(1)}$$

Where:

E_f : The field efficiency.

C_{ef} ; effective field capacity in m^2 / h .

C_{th} : theoretical e field capacity in m^2 / h .

$$C_{th} = S \cdot W / 4200 \text{-----(2)}$$

Where:

S = travel speed , in m / h .

W = operating width of the mower in m.

The effective field capacity (C_{ef}) is the actual average working rate of area concerning the amount of time lost during the operation.

2 - Shearing efficiency:

Shearing efficiency was calculated by using the following formula.

$$E_c = \frac{A - B}{A} \times 100 \text{-----(3)}$$

Where

A : height of turf grass stalks above the soil service before cutting, in cm.

B : height of turf grass stalks above the soil after cutting, cm.

3 - Power requirements:

The power can be calculated by measuring fuel consumption and by using the following equation.

$$E_p = \{F_c \} \times LCV \times 427 \eta_{th} \times \eta_m \text{----- (4)}$$

Where:

F_c : The fuel consumption, Kg / h

LCV: The lower calorific value of fuel (kJ / kg), average LCV of gasoline is 11000 kcal/kg.

η_m: mechanical efficiency of the about 80 % for gasoline engine

η_{th}: The thermal efficiency of the engine, (consider to be about 25 % for gasoline engine)

100: Thermal-mechanical equivalent, kg .m/kJ.

Hence, the specific energy consumed can be calculated as follows:

$$C_E = (E_p / C_{ef}) , kW .h / m^2 \text{-----(5)}$$

Where:

E_p: power requirement, kW.

C_{ef} ; effective field capacity in m² / h

4 - Operation cost:

The operation costs of the mower were calculated according to (Awady 1978).

$$C = p / h (1/e + i/2 + t + r) + (1.2 kW . F S) + W / 144 \text{--(6)}$$

Where:

C : is the hourly cost, LE / h

p : is the capital investment.(750 L .E)

h : is the yearly operating hours, (1000 h/ year)

e : is life expectancy of equipment in year (10 year)..

i : is the interest rate,(10 %)

t : is the taxes and overheads (2 %).

r : is the repairs ratio of the total investment.(10 %)

1.2: is a factor including reasonable estimation of the oil consumption in addition to fuel.

F : is the specific fuel consumption, (0.9 L / kW .h).

S : is the price of fuel per liter (2.35 L .E) .

w : is the labor wage rate per month (500 L.E).

144 : is the reasonable estimation of monthly working hours

RESULTS AND DISCUSSION

The influences of some operating parameters on the performance of turf grass shear machine are discussed as follows:

Effect of kinematic parameter on field efficiency:

Representative values of field efficiency versus portable machine kinematic parameters with knife types(imported and modified) and blade number (three and four blade) are given in Fig. 2.

Results show that, field efficiency values were increased as the kinematic parameters increased. Data obtained show that increased the portable machine kinematic parameters from 180 to 290, increased the field efficiency by 81.2 to 98.6 % with modified knife with blades three. Decreased at the lower values of kinematic parameters, the field efficiency was 72.2 at 180 kinematic parameters and 86.5 at the 290 kinematic parameters for the imported knife with blades four.

The major reason for the increase in field efficiency by increasing the kinematic parameters is due to the less theoretical time consumed in comparison with the other items of time losses.

Influence of some operating parameters on cutting efficiency:

Cutting efficiency is greatly affected by many operating parameters. Unadjustment of these parameters caused a serious turf grass damage that tends to increase losses, and in turn decreased turf grass quality, (Fig.3).

Representative values of cutting efficiency versus portable machine kinematic parameters with knife types(imported and modified) and blade number (three and four blade) are given in Fig.3.

Results show that cutting efficiency values were increased as the kinematic parameters increased. Data obtained show that increased the portable machine kinematic parameters from 180 to 290, increased the cutting efficiency by 93.3 and 98.5 % with modified knife with blades three. Decreased at the lower values of kinematic parameters.

The cutting efficiency was 85.3 at 180 kinematic parameters and 90.2 at the 290 kinematic parameters for the imported knife with blades four.

The major reason for the increase in cutting efficiency by increasing the kinematic parameters.

The increase of cutting height with the decrease of kinematic parameter is due to bending of turf grass under the cutter disk of the portable machine, added to that, a great number of plants were left without cutting, resulting in a remarkable drop in cutting efficiency.

Effect of kinematic parameter on specific energy consumption:

Specific energy consumption as related to the kinematic parameters with knife types (imported and modified) and blade number (three and four blade).

Fig. 4 shows that the specific energy consumption decreased as the kinematic parameters increased. Increased the portable machine kinematic parameters from 180 to 290 increased the fuel consumption by 20.6 and 17.7 kW . h / fed with modified knife with blades three.. Decreased at the lower values of kinematic parameters. The specific energy consumption was 25.7 kW . h/ fed at 180 kinematic parameters and 22.9 kW . h/ fed at the 290 kinematic parameters for the imported knife with blades four. The decrease of specific energy consumption by increasing the kinematic parameter is attributed to the increase of field capacity, results in low values of fuel per feddan.

Cost of using the machine:

The operating cost was determined 78 L.E / fed with knife modified and blade number three.

CONCLUSION

- The proper adjustment of the portable machine kinematic parameter during the shearing operation is of great importance to increase the field capacity and decrease cost requirements.
- Increasing the portable machine kinematic parameter from 180 to 290, increased the field efficiency by 81.2 to 98.6 % with knife modified and blade number three, increased the cutting efficiency by 93.2 and 98.5 % with knife modified and blade number three, and decreased the specific energy consumption by 20.6 and 17.7 kW.h/ fed with knife modified and blade number three .
- Rotary portable machine kinematic parameter of 290 minimized the mowing costs.

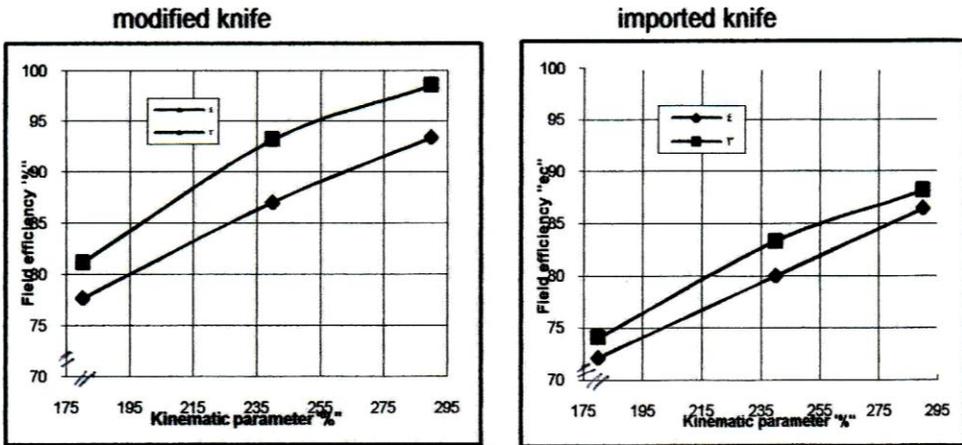


Fig (2): Effect of kinematic parameter "y" on the field efficiency "Ec" at different knife types and blade number.

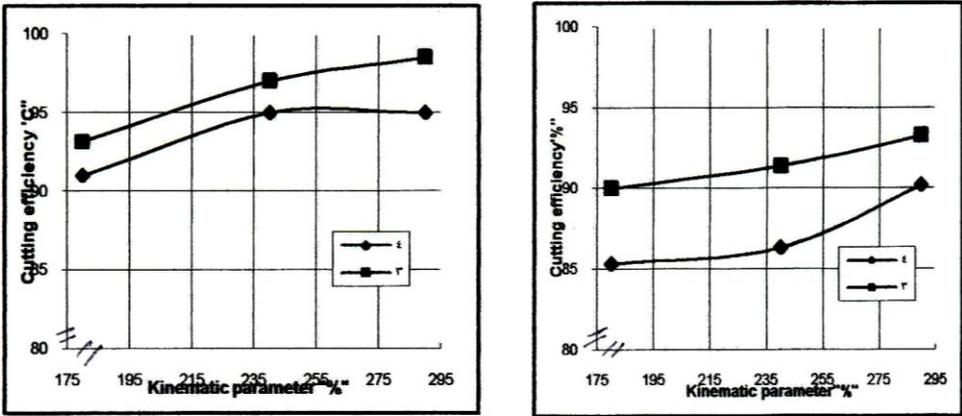


Fig (3): Effect of kinematic parameter "y" on the cutting efficiency "C" at different knife types and blade number.

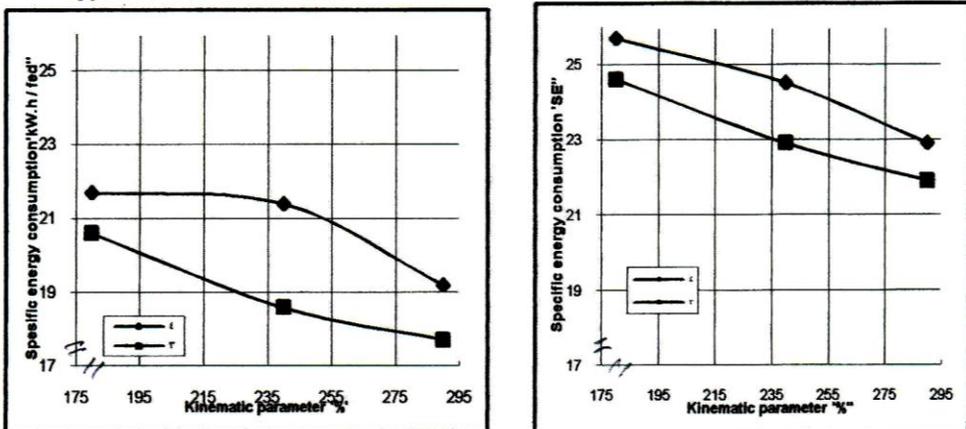


Fig. (4): Effect of kinematic "y" on the specific energy consumption "SE" at different knife types and blade number.

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الملخص العربي**تقييم أداء آلة محمولة لقص النجيل****د / رأفت علي أحمد وربى**

في السنوات الأخيرة تم الاهتمام بزراعة المدن والقرى السياحية والفنادق والنوادي والملاعب والطرق وملاعب الجولف والمنشآت الحكومية وبناء على هذا التوسع زادت المسطحات الخضراء التي تحتاج إلي قص علي فترات مختلفة خاصة في المساحات الصغيرة. ولذلك يهدف البحث إلى استخدام آلة محمولة لقص النجيل في المساحات الصغيرة وتقييم أدائها من خلال المتغيرات الآتية:

أستاذ المساعد - قسم هندسة الآلات والقوي الزراعية - كلية الهندسة الزراعية - جامعة الأزهر - القاهرة

علاقة السرعة الدورانية للسكاكين إلى السرعة الأمامية للألة (المعامل الكينماتيكي - ١) واستخدام أنواع من الأسلحة المستوردة ذات الشفرات الثابتة والأسلحة المحلية الصنع ذات الشفرات الحرة مع استخدام ثلاث وأربع شفرات علي الرأس القاطعة. ومحاولة دراسة تأثير ذلك على أداء الألة.

وقد تم تقييم أداء الألة من حيث:

- معدل الأداء والكفاءة الحقلية
 - ارتفاع القطع وكفاءة القطع
 - استهلاك الوقود والطاقة النوعية المطلوبة
 - تكاليف التشغيل
- وتم القص عند نسبة رطوبة للنجيل ٤٠ % وارتفاع قطع ٤ سم من سطح الأرض.

وقد وجد من تحليل النتائج ما يلي:

- تزداد كفاءة الألة الحقلية كلما زاد المعامل الكينماتيكي مع نوعي أسلحة القطع المستخدمة ومع ثلاث شفرات للقطع. وكانت اعلي كفاءة حقلية ٨١,٢ % عند معامل كينماتيكي ١٨٠ وكانت ٩٨,٦ % عند معامل كينماتيكي ٢٩٠ مع استخدام سلاح قطع معدل و٣ شفرات حر الحركة. وكانت اقل كفاءة حقلية ٧٢,٢ % عند معامل كينماتيكي ١٨٠ وكانت ٨٦,٥ % عند معامل كينماتيكي ٢٩٠ مع استخدام سلاح قطع مستورد ذو ٤ شفرة ثابتة.

- يقل ارتفاع القطع وتزيد كفاءة القطع كلما زاد المعامل الكينماتيكي مع نوعي أسلحة القطع المستخدمة ومع ثلاث شفرات للقطع. وكانت اعلي كفاءة قطع ٩٣,٢ % عند معامل كينماتيكي ١٨٠ وكانت ٩٨,٥ % عند معامل كينماتيكي ٢٩٠ مع استخدام سلاح قطع معدل و٣ شفرات حر الحركة. وكانت اقل كفاءة قطع ٨٥,٣ % عند معامل كينماتيكي ١٨٠ وكانت ٩٠,٢ % عند معامل كينماتيكي ٢٩٠ مع استخدام سلاح قطع مستورد ذو ٤ شفرة ثابتة.

- وكانت الطاقة النوعية المطلوبة تقل مع زيادة المعامل الكينماتيكي مع أسلحة القطع المستخدمة. وكانت اقل طاقة نوعية عند معامل كينماتيكي ٢٩٠ هو ١٧,٧ كيلوات . ساعة / فدان مع استخدام سلاح معدل و٣ شفرات حرة، وكانت اكبر طاقة نوعية ٢٥,٧ كيلوات . ساعة / فدان عند معامل كينماتيكي ١٨٠ مع استخدام سلاح مستورد و ٤ شفرة ثابتة

ونوصي باستخدام الألة عند معامل كينماتيكي ٢٩٠ مع استخدام سلاح معدل ذو ثلاث شفرات للقطع ليعطي اعلي كفاءة حقلية واعلي كفاءة قطع مع اقل التكاليف.